

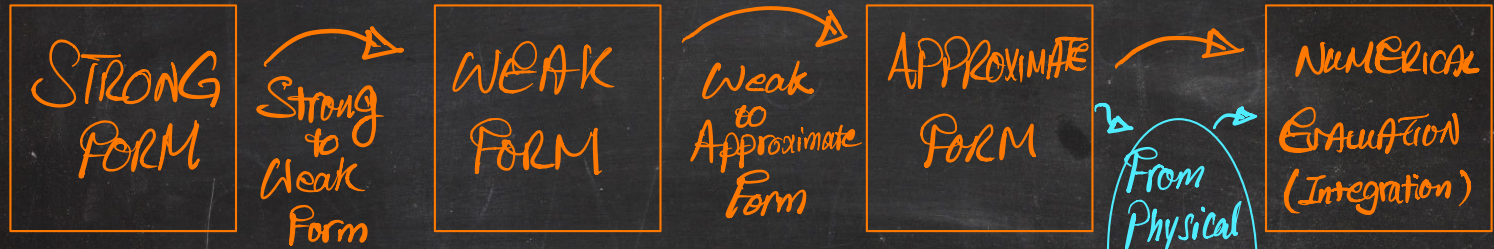
# FINITE ELEMENT METHOD

FINITE ELEMENT METHOD

23

# FINITE ELEMENT METHOD

Differential Equation  $\star$



ROADMAP FOR FEM

1D  
2D

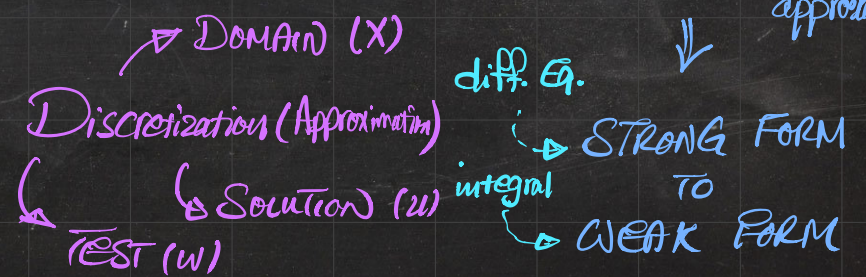
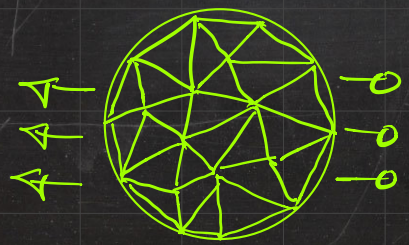
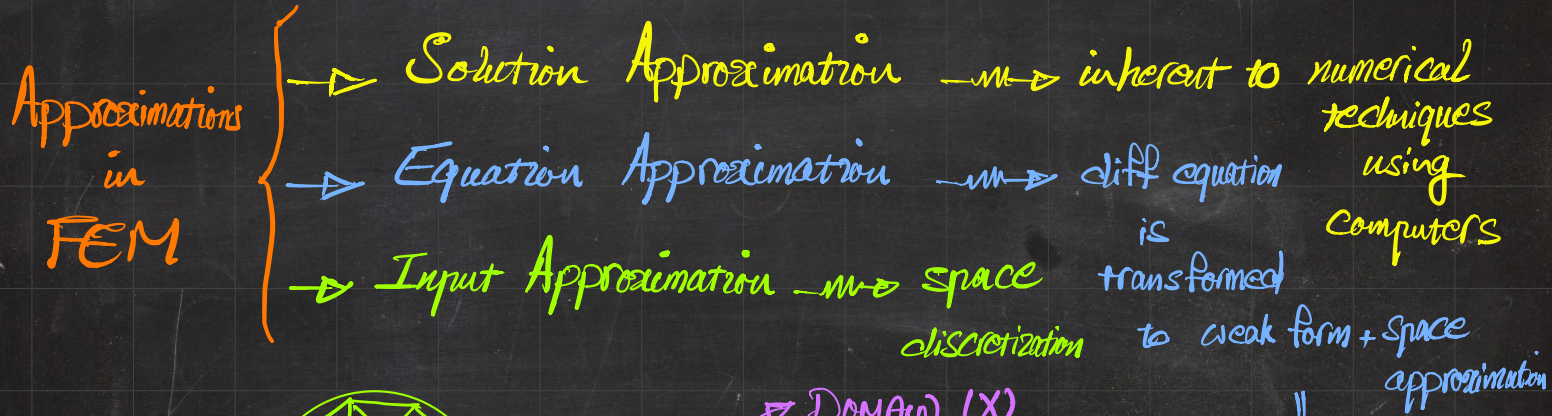
DISCRETIZED FORM

APPROXIMATION TECHNIQUES  
SHAPE FUNCTIONS

Approximate Solution to Differential Equation  $\star$



# UNDERSTANDING FEM VIA AN ANALOGY (A BRUTAL SIMPLIFICATION)



# 1D FEM

## Overview and Wrap-up

# FINITE ELEMENT METHOD IN A NUTSHELL

Diff. Eq.  $(EAu')' + b = 0$   
 2ND. O.D.E.

**STRONG FORM**

(I) MULTIPLY BY  $w$  (test function)  
 (II) INTEGRATE

**WEAK FORM**

INTEGRAL FORM

$$\int_0^1 w'u' dx = \int_0^1 w da + w(1)u'(1) - w(0)u'(0)$$

PIECEWISE

**APPROXIMATE FORM**

Approximate Discretized Weak Form

Approximation

**DISCRETIZED FORM**

NUMERICAL INTEGRATION  
 another source of approx...

**ELEMENT-WISE QUANTITIES**

**SOLVE**

PostProcess

**GLOBAL SYSTEM**

FROM GLOBAL TO ELEMENTS

FROM INTEGRAL OVER THE DOMAIN TO SUBINTEGRALS

$$\int_0^1 \dots dx = \int_0^a \dots dx + \int_a^b \dots dx + \dots$$

$$[K][u] = [F]$$

**ASSEMBLY**

PIECEWISE INTEGRALS (SOLUTIONS)



# FROM STRONG FORM TO ELEMENT STIFFNESS IN PHYSICAL SPACE

$EA u'' = 0$  SUBJECT TO BCs



MULTIPLY BY  
TEST  
FUNCTION  
 $w$

$\left\{ \begin{array}{l} \text{DIRICHLET} \rightarrow u \text{ IS PRESCRIBED} \\ \text{NEUMANN} \rightarrow u' \text{ IS PRESCRIBED} \end{array} \right.$

$EA w u'' = 0 \rightarrow w u'' = (w u')' - w' u'$

$EA [(w u')' - w' u'] = 0 \Rightarrow EA w' u' = EA (w u')'$  INTEGRATE

$\int_L EA w' u' dx = \int_L EA (w u')' dx = EA w u' \Big|_{\text{1}}^{\text{2}} = EA w^2 u'^2 - EA w^1 u'^1$

FROM STRONG FORM TO ELEMENT STIFFNESS  $\rightarrow$  IN PHYSICAL SPACE NO.23

$EA u'' = 0$  SUBJECT TO BCs



$$EA \begin{bmatrix} \int_L N^1{}' N^1{}' dx & \int_L N^1{}' N^2{}' dx \\ \int_L N^2{}' N^1{}' dx & \int_L N^2{}' N^2{}' dx \end{bmatrix} \begin{bmatrix} u^1 \\ u^2 \end{bmatrix} = \begin{bmatrix} F^1 \\ F^2 \end{bmatrix}$$

$$\begin{bmatrix} K^{11} & K^{12} \\ K^{21} & K^{22} \end{bmatrix} \begin{bmatrix} u^1 \\ u^2 \end{bmatrix} = \begin{bmatrix} F^1 \\ F^2 \end{bmatrix} \quad \rightarrow \quad K^{ij} = EA \int_L N^i{}' N^j{}' dx$$

$$K^{ij} = EA \int_L n^i n^j dx$$

PHYSICAL RECALL:

$$= EA \int_{-1}^1 \frac{\partial n^i}{\partial \xi} \frac{\partial n^j}{\partial \xi} J^{-1} d\xi$$

NATURAL

$$\int_{-1}^1 g(\xi) d\xi = \sum_{gp=1}^{GPE} g(\xi) \alpha_{gp}$$

Loop over gp

$$= EA \sum_{gp=1}^{GPE} \left\{ \left[ \frac{\partial n^i}{\partial \xi} \frac{\partial n^j}{\partial \xi} J^{-1} \right]_{gp} \times \alpha_{gp} \right\}$$

END

WHAT YOU SEE IN THE CODE!

For gp=1:GPE  
 ...  
 End

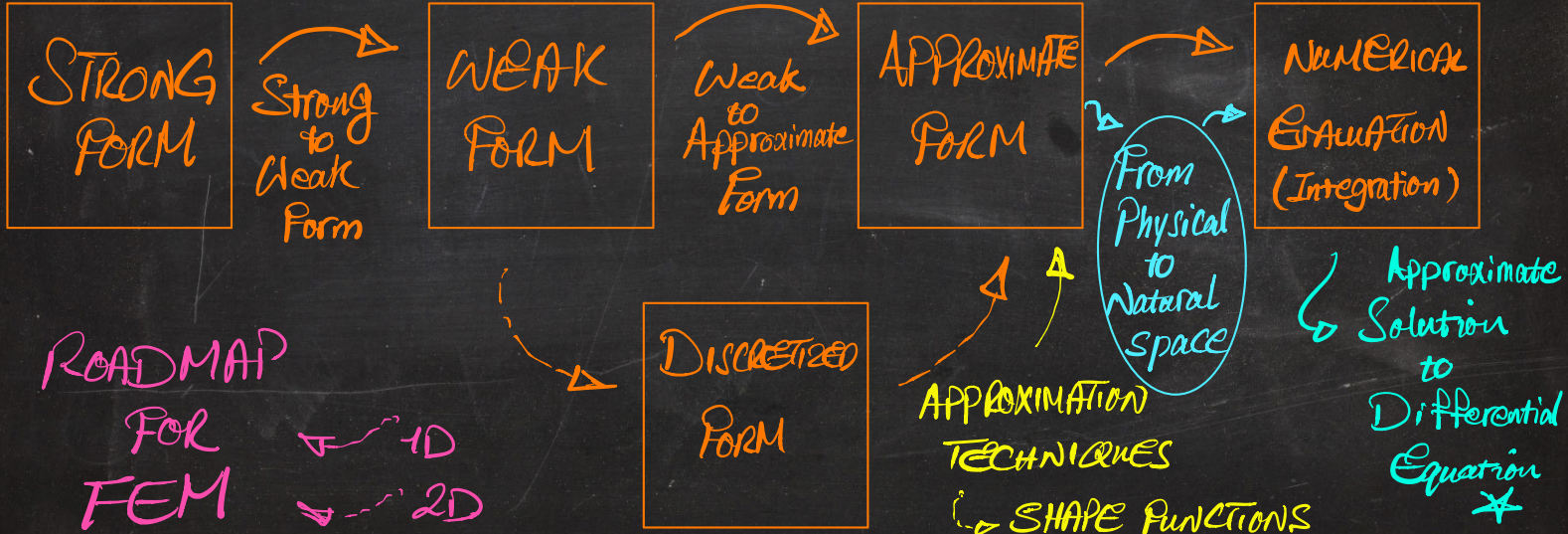
eg. in MATLAB



# 2D FEM

# FINITE ELEMENT METHOD

Differential Equation \*



# MATHEMATICAL PRELIMINARIES



# EINSTEIN SUMMATION CONVENTION

↪ A little definition for notation convenience

↪ A REPEATED INDEX TWICE MEANS SUMMATION OVER THAT INDEX

also, called "dummy index"

$$\sum_{i=1}^3 u_i v_i = u_1 v_1 + u_2 v_2 + u_3 v_3 \equiv u_i v_i \quad \swarrow \text{ } i \text{ is summation index}$$

$i$ : free index

$$\sum_{j=1}^3 A_{ij} u_j \Rightarrow \begin{cases} i=1 \Rightarrow A_{11} u_1 + A_{12} u_2 + A_{13} u_3 \\ i=2 \Rightarrow A_{21} u_1 + A_{22} u_2 + A_{23} u_3 \\ i=3 \Rightarrow A_{31} u_1 + A_{32} u_2 + A_{33} u_3 \end{cases} \Rightarrow \begin{bmatrix} A_{11} & A_{12} & A_{13} \\ A_{21} & A_{22} & A_{23} \\ A_{31} & A_{32} & A_{33} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} \equiv A_{ij} u_j$$

$j$ : summation index

$$u \cdot v = u_x v_x + u_y v_y + u_z v_z = u_1 v_1 + u_2 v_2 + u_3 v_3 = \sum_{i=1}^3 u_i v_i = u_i v_i$$

↳ Dot Product ( $u, v$ )  $\mapsto$  SCALAR  $\leftarrow u_i v_i \leftarrow u \cdot v$

Double Dot Product ( $A, B$ )  $\mapsto$  SCALAR  $\leftarrow A_{ij} B_{ij} \leftarrow A : B$

$u \otimes v$  Dyadic Product ( $u, v$ )  $\mapsto$  MATRIX  $\leftarrow u_i v_j \leftarrow [u \otimes v]_{ij}$

KRONECKER DELTA  $\mapsto \delta_{ij} = \phi_i \cdot \phi_j \Rightarrow \begin{cases} 1 & i=j \\ 0 & i \neq j \end{cases}$

$$u \cdot v = u_i v_i \quad [A \cdot B]_{ik} = A_{ij} B_{jk} \quad [u \otimes v]_{ij} = u_i v_j$$

$$\delta_{ij} = \phi_i \cdot \phi_j \quad [A \cdot u]_i = A_{ij} u_j \quad A \circ B = A_{ij} B_{ij}$$

$E$  is FOURTH-ORDER TENSOR (ARRAY) is  $3 \times 3 \times 3 \times 3 = 81$  Components

$\swarrow$  2nd.     $\swarrow$  4th.     $\swarrow$  2nd.  
 $B = E \circ \Phi \quad m \rightarrow [B]_{ij} = [E]_{ijkl} [\Phi]_{kl}$

INSTEAD OF  $x, y, z$   $m \rightarrow 1, 2, 3$  is  $x_1, x_2, x_3$      $\phi_x \sim \phi_1$



SCALAR  $\rightarrow 0$ , VECTOR  $\rightarrow 1$ , MATRIX  $\rightarrow 2$

$$\text{GRAD } \Phi = \begin{bmatrix} \partial\Phi/\partial x_1 \\ \partial\Phi/\partial x_2 \\ \partial\Phi/\partial x_3 \end{bmatrix}$$

$$\text{GRAD } u = \begin{bmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{bmatrix}$$

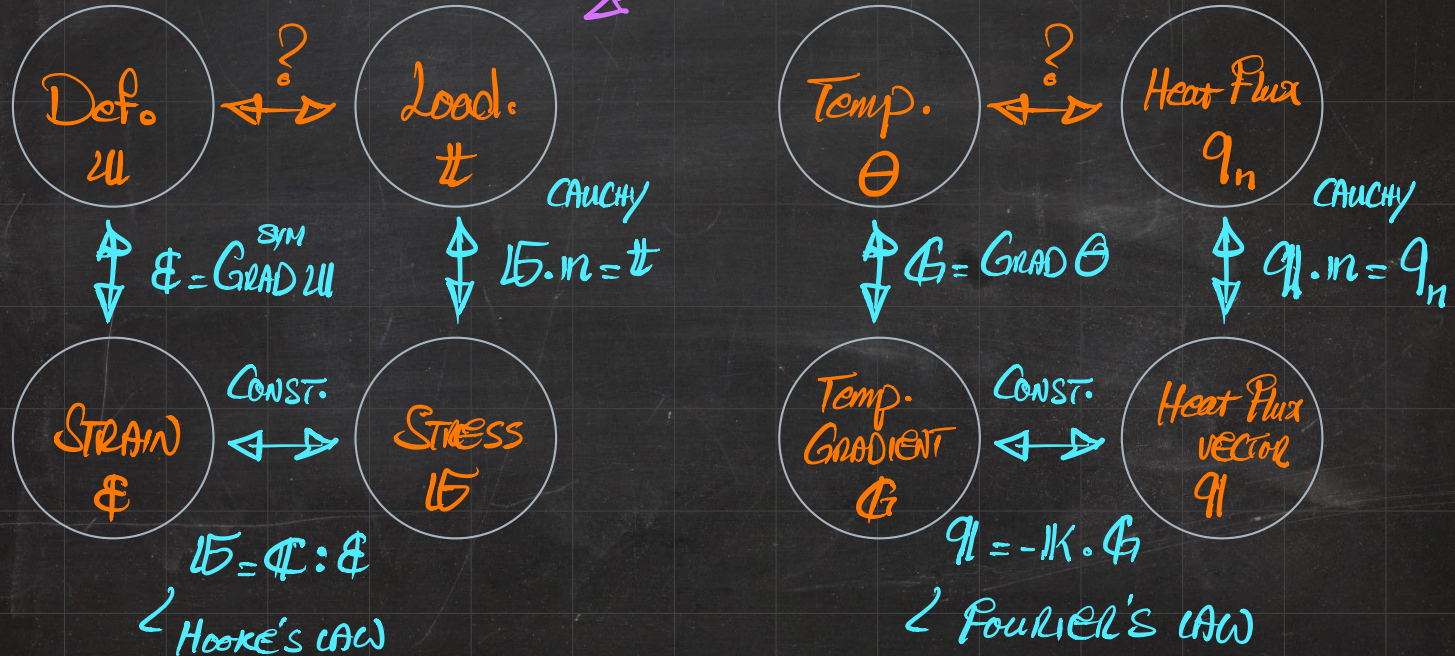
$$\text{DIV } u = \frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} + \frac{\partial u_3}{\partial x_3}$$

$$\text{DIV } A = \begin{bmatrix} \frac{\partial A_{11}}{\partial x_1} + \frac{\partial A_{12}}{\partial x_2} + \frac{\partial A_{13}}{\partial x_3} \\ \frac{\partial A_{21}}{\partial x_1} + \frac{\partial A_{22}}{\partial x_2} + \frac{\partial A_{23}}{\partial x_3} \\ \frac{\partial A_{31}}{\partial x_1} + \frac{\partial A_{32}}{\partial x_2} + \frac{\partial A_{33}}{\partial x_3} \end{bmatrix}$$

GRADIENT INCREASES  
THE ORDER BY 1

DIVERGENCE REDUCES  
THE ORDER BY 1

# Big Picture of Mechanics (Mechanical Problems & Thermal Problems)



STRONG FORM (GENERIC FORM)  $\rightarrow \text{Div } \mathbf{B} + \mathbf{b} = 0$ ,  $\text{Div } \mathbf{q} + c = 0$

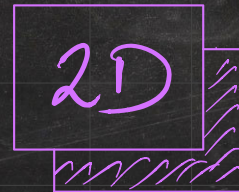
$$\frac{\partial B_{jk}}{\partial x_k} + b_j = 0$$

$$\frac{\partial q_i}{\partial x_i} + c = 0$$

$$\begin{cases} \frac{\partial B_{xx}}{\partial x} + \frac{\partial B_{xy}}{\partial y} + b_x = 0 \\ \frac{\partial B_{yx}}{\partial x} + \frac{\partial B_{yy}}{\partial y} + b_y = 0 \end{cases}$$

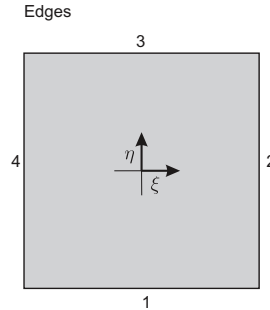
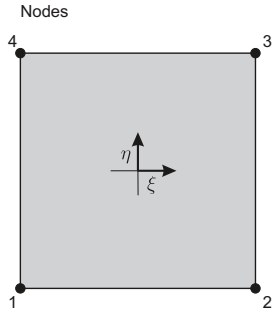
$$\frac{\partial q_x}{\partial x} + \frac{\partial q_y}{\partial y} + c = 0$$

2D  $\rightarrow$  Plane STRAIN }  $\mathbf{B} = \mathbf{F} \cdot \mathbf{B}$   
 Plane STRESS }





- two-dimensional 4-noded quadrilateral element (D2QU4N)  
a.k.a. bilinear quadrilateral element
- two-dimensional 9-noded quadrilateral element (D2QU9N)  
a.k.a. Lagrange biquadratic quadrilateral element
- two-dimensional 8-noded quadrilateral element (D2QU8N)  
a.k.a. serendipity biquadratic quadrilateral element
- two-dimensional 3-noded triangular element (D2TR3N)  
a.k.a. constant strain triangle
- two-dimensional 6-noded triangular element (D2TR6N)  
a.k.a. quadratic triangle
- two-dimensional quadrature rule



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1

$$N^1 = \frac{1}{4} (1 - \xi) (1 - \eta)$$

$$N_{,\xi}^1 = -\frac{1}{4} (1 - \eta)$$

$$N_{,\eta}^1 = -\frac{1}{4} (1 - \xi)$$

$$N^2 = \frac{1}{4} (1 + \xi) (1 - \eta)$$

$$N_{,\xi}^2 = +\frac{1}{4} (1 - \eta)$$

$$N_{,\eta}^2 = -\frac{1}{4} (1 + \xi)$$

$$N^3 = \frac{1}{4} (1 + \xi) (1 + \eta)$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + \eta)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi)$$

$$N^4 = \frac{1}{4} (1 - \xi) (1 + \eta)$$

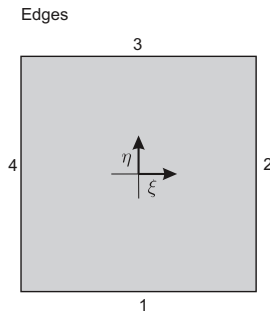
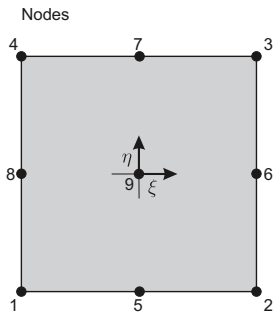
$$N_{,\xi}^4 = -\frac{1}{4} (1 + \eta)$$

$$N_{,\eta}^4 = +\frac{1}{4} (1 - \xi)$$

# 2D Finite Element Library

## D2QU9N

## Lagrange biquadratic quadrilateral element



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1
5	0	-1
6	1	0
7	0	1
8	-1	0
9	0	0

$$N^1 = +\frac{1}{4} (1 - \xi) \xi (1 - \eta) \eta$$

$$N^2 = -\frac{1}{4} (1 + \xi) \xi (1 - \eta) \eta$$

$$N^3 = +\frac{1}{4} (1 + \xi) \xi (1 + \eta) \eta$$

$$N^4 = -\frac{1}{4} (1 - \xi) \xi (1 + \eta) \eta$$

$$N^5 = -\frac{1}{2} (1 - \xi) (1 + \xi) (1 - \eta) \eta$$

$$N^6 = +\frac{1}{2} (1 + \xi) \xi (1 - \eta) (1 + \eta)$$

$$N^7 = +\frac{1}{2} (1 - \xi) (1 + \xi) (1 + \eta) \eta$$

$$N^8 = -\frac{1}{2} (1 - \xi) \xi (1 - \eta) (1 + \eta)$$

$$N^9 = (1 - \xi) (1 + \xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^1 = +\frac{1}{4} (1 - 2\xi) (1 - \eta) \eta$$

$$N_{,\xi}^2 = -\frac{1}{4} (1 + 2\xi) (1 - \eta) \eta$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + 2\xi) (1 + \eta) \eta$$

$$N_{,\xi}^4 = -\frac{1}{4} (1 - 2\xi) (1 + \eta) \eta$$

$$N_{,\xi}^5 = \xi \eta (1 - \eta)$$

$$N_{,\xi}^6 = \frac{1}{2} (1 + 2\xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^7 = -\xi \eta (1 + \eta)$$

$$N_{,\xi}^8 = -\frac{1}{2} (1 - 2\xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^9 = -2\xi (1 - \eta) (1 + \eta)$$

$$N_{,\eta}^1 = +\frac{1}{4} (1 - \xi) \xi (1 - 2\eta)$$

$$N_{,\eta}^2 = -\frac{1}{4} (1 + \xi) \xi (1 - 2\eta)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi) \xi (1 + 2\eta)$$

$$N_{,\eta}^4 = -\frac{1}{4} (1 - \xi) \xi (1 + 2\eta)$$

$$N_{,\eta}^5 = \frac{1}{2} (1 - \xi) (1 + \xi) (2\eta - 1)$$

$$N_{,\eta}^6 = -(1 + \xi) \xi \eta$$

$$N_{,\eta}^7 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 + 2\eta)$$

$$N_{,\eta}^8 = (1 - \xi) \xi \eta$$

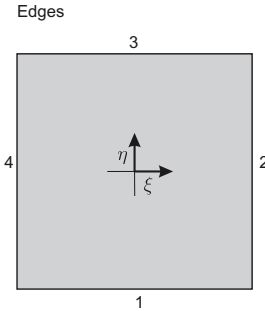
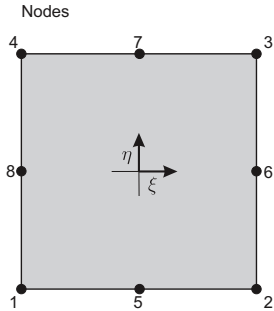
$$N_{,\eta}^9 = -2(1 - \xi) (1 + \xi) \eta$$



# 2D Finite Element Library

## D2QU8N

## serendipity biquadratic quadrilateral element



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1
5	0	-1
6	1	0
7	0	1
8	-1	0

$$N^1 = -\frac{1}{4} (1 - \xi) (1 - \eta) (1 + \xi + \eta)$$

$$N^2 = -\frac{1}{4} (1 + \xi) (1 - \eta) (1 - \xi + \eta)$$

$$N^3 = -\frac{1}{4} (1 + \xi) (1 + \eta) (1 - \xi - \eta)$$

$$N^4 = -\frac{1}{4} (1 - \xi) (1 + \eta) (1 + \xi - \eta)$$

$$N^5 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 - \eta)$$

$$N^6 = \frac{1}{2} (1 + \xi) (1 + \eta) (1 - \eta)$$

$$N^7 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 + \eta)$$

$$N^8 = \frac{1}{2} (1 - \xi) (1 + \eta) (1 - \eta)$$

$$N_{,\xi}^1 = +\frac{1}{4} (1 - \eta) (2\xi + \eta)$$

$$N_{,\xi}^2 = +\frac{1}{4} (1 - \eta) (2\xi - \eta)$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + \eta) (2\xi + \eta)$$

$$N_{,\xi}^4 = +\frac{1}{4} (1 + \eta) (2\xi - \eta)$$

$$N_{,\xi}^5 = -\xi (1 - \eta)$$

$$N_{,\xi}^6 = +\frac{1}{2} (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^7 = -\xi (1 + \eta)$$

$$N_{,\xi}^8 = -\frac{1}{2} (1 - \eta) (1 + \eta)$$

$$N_{,\eta}^1 = +\frac{1}{4} (1 - \xi) (\xi + 2\eta)$$

$$N_{,\eta}^2 = +\frac{1}{4} (1 + \xi) (-\xi + 2\eta)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi) (\xi + 2\eta)$$

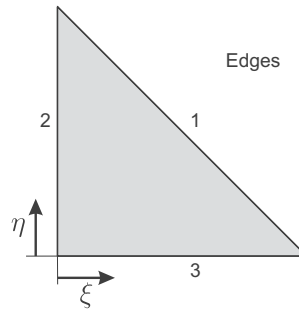
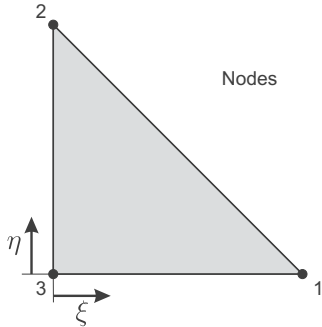
$$N_{,\eta}^4 = +\frac{1}{4} (1 - \xi) (-\xi + 2\eta)$$

$$N_{,\eta}^5 = -\frac{1}{2} (1 - \xi) (1 + \xi)$$

$$N_{,\eta}^6 = -(1 + \xi) \eta$$

$$N_{,\eta}^7 = +\frac{1}{2} (1 - \xi) (1 + \xi)$$

$$N_{,\eta}^8 = -(1 - \xi) \eta$$



Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$$N^1 = \xi$$

$$N^2 = \eta$$

$$N^3 = (1 - \xi - \eta)$$

$$N^1_{,\xi} = 1$$

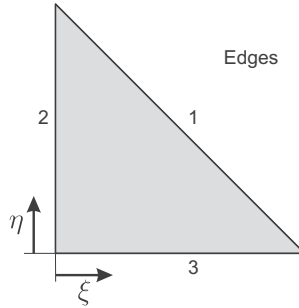
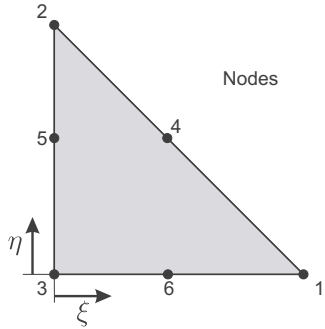
$$N^2_{,\xi} = 0$$

$$N^3_{,\xi} = -1$$

$$N^1_{,\eta} = 0$$

$$N^2_{,\eta} = 1$$

$$N^3_{,\eta}(\xi, \eta) = -1$$



Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0
4	1/2	1/2
5	0	1/2
6	1/2	0

$$N^1 = \xi(2\xi - 1)$$

$$N_{,\xi}^1 = -1 + 4\xi$$

$$N_{,\eta}^1 = 0$$

$$N^2 = \eta(2\eta - 1)$$

$$N_{,\xi}^2 = 0$$

$$N_{,\eta}^2 = -1 + 4\eta$$

$$N^3 = (1 - \xi - \eta)(1 - 2\xi - 2\eta)$$

$$N_{,\xi}^3 = -3 + 4\xi + 4\eta$$

$$N_{,\eta}^3 = -3 + 4\xi + 4\eta$$

$$N^4 = 4\xi\eta$$

$$N_{,\xi}^4 = 4\eta$$

$$N_{,\eta}^4 = 4\xi$$

$$N^5 = 4\eta(1 - \xi - \eta)$$

$$N_{,\xi}^5 = -4\eta$$

$$N_{,\eta}^5 = -4(-1 + 2\eta + \xi)$$

$$N^6 = 4\xi(1 - \xi - \eta)$$

$$N_{,\xi}^6 = -4(-1 + \eta + 2\xi)$$

$$N_{,\eta}^6 = -4\xi$$



## two-dimensional quadrature rule i

### Triangular Elements Gauss Point Rule

$$\int_0^1 \int_0^{1-\eta} \{\bullet\} d\xi d\eta \approx \frac{1}{2} \sum_{i=1}^{N_{\text{Gauss Points}}} \alpha_i \{\bullet\}_{\text{Gauss Point } i}$$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/3	1/3	1

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/6	1/6	1/3
2	4/6	1/6	1/3
3	1/6	4/6	1/3

## two-dimensional quadrature rule ii

### Quadrilateral Elements Gauss Point Rule

$$\int_{-1}^1 \int_{-1}^1 \{\bullet\} d\xi d\eta \approx \sum_{i=1}^{N_{\text{Gauss Points}}} \alpha_i \{\bullet\}_{\text{Gauss Point } i}$$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	0	0	$2 \times 2$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	$-1/\sqrt{3}$	$-1/\sqrt{3}$	$1 \times 1$
2	$+1/\sqrt{3}$	$-1/\sqrt{3}$	$1 \times 1$
3	$+1/\sqrt{3}$	$+1/\sqrt{3}$	$1 \times 1$
4	$-1/\sqrt{3}$	$+1/\sqrt{3}$	$1 \times 1$

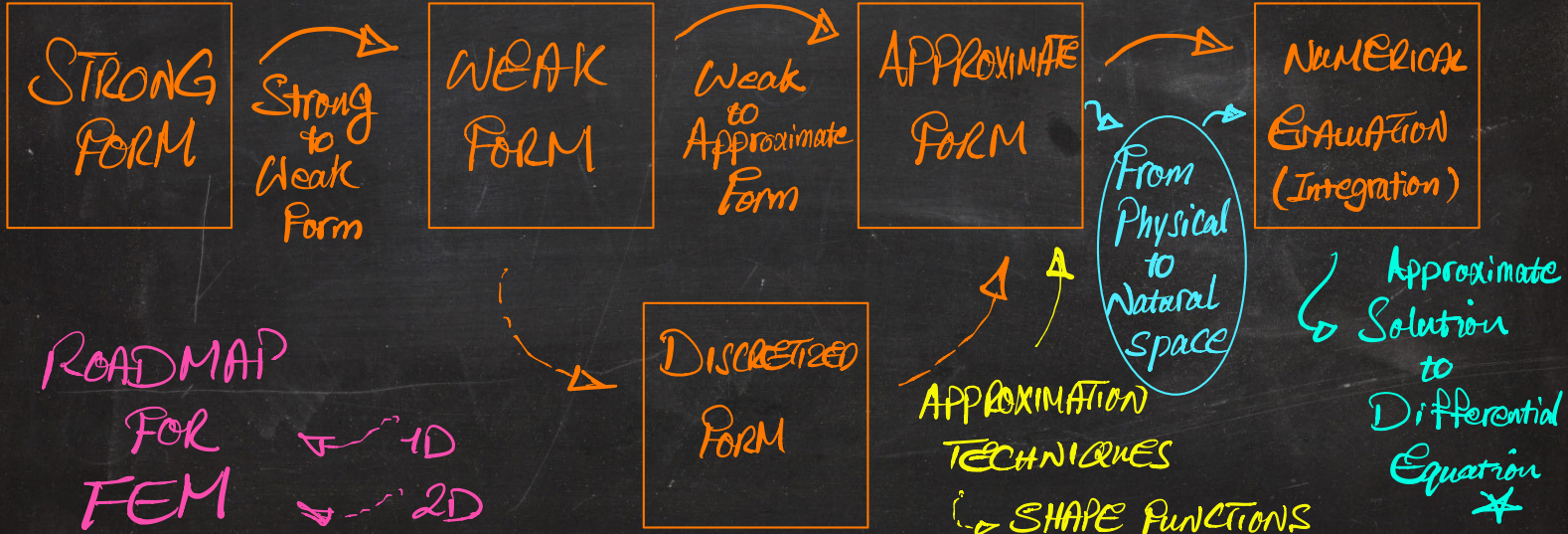
## two-dimensional quadrature rule iii

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	$-\sqrt{3/5}$	$-\sqrt{3/5}$	$5/9 \times 5/9$
2	$+\sqrt{3/5}$	$-\sqrt{3/5}$	$5/9 \times 5/9$
3	$\sqrt{3/5}$	$\sqrt{3/5}$	$5/9 \times 5/9$
4	$-\sqrt{3/5}$	$\sqrt{3/5}$	$5/9 \times 5/9$
5	0	$-\sqrt{3/5}$	$5/9 \times 8/9$
6	$+\sqrt{3/5}$	0	$5/9 \times 8/9$
7	0	$\sqrt{3/5}$	$5/9 \times 8/9$
8	$-\sqrt{3/5}$	0	$5/9 \times 8/9$
9	0	0	$8/9 \times 8/9$

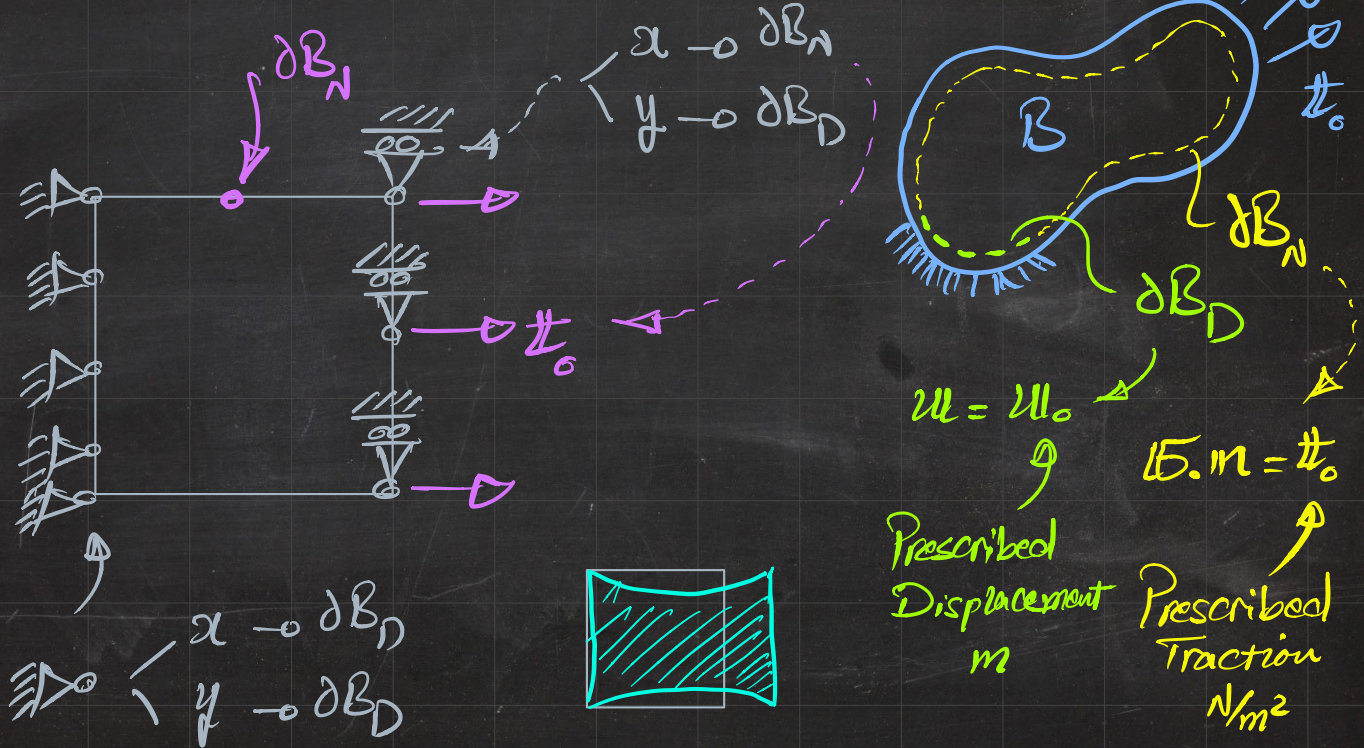


# FINITE ELEMENT METHOD

Differential Equation \*



# FROM STRONG FORM TO WEAK FORM

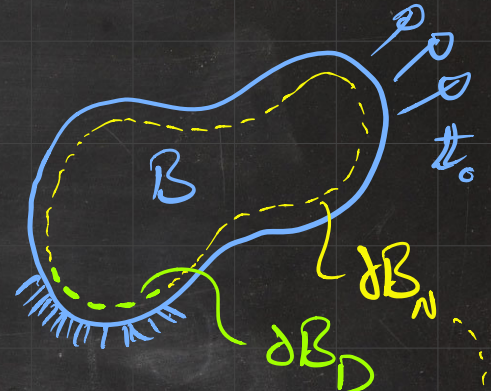


# FROM STRONG FORM TO WEAK FORM

$\text{Div } \mathbf{E} = \phi$  in  $B$  subject to BCs

⊙ STRONG FORM IN THE ABSENCE OF BODY FORCES

⊙  $u = u_0$  at  $\partial B_D$   
 $\mathbf{E} \cdot \mathbf{n} = t_0$  at  $\partial B_N$



$u = u_0$  ⊙ Prescribed Displacement  $m$   
 $\mathbf{E} \cdot \mathbf{n} = t_0$  ⊙ Prescribed Traction  $N/m^2$

⊙  $\text{Div } \mathbf{E} = 0$  (dot) SCALAR

⊙ TEST FUNCTION

⊙  $\forall w$

$w|_{\partial B_D} = 0$



# FROM STRONG FORM TO WEAK FORM

$$u = u_0 \quad \text{at } \partial B_D$$

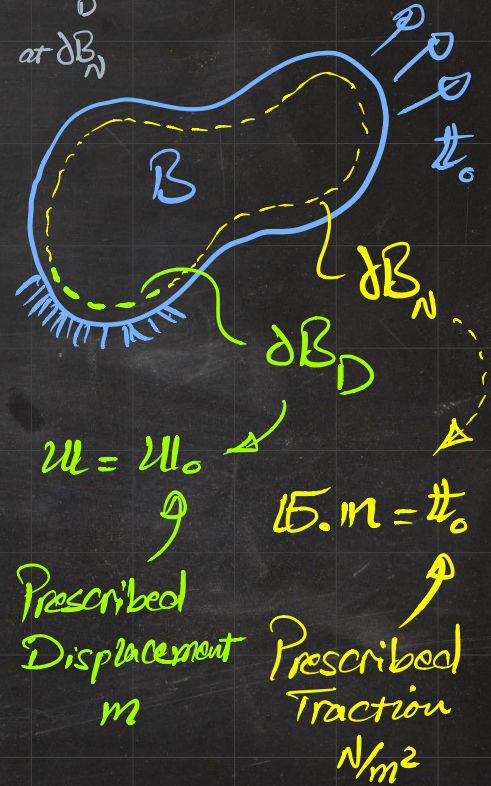
$$\mathbf{B} \cdot \mathbf{n} = \mathbf{t}_0 \quad \text{at } \partial B_N$$

$\text{Div } \mathbf{B} = \phi$  in  $B$  subject to BCs

w.  $\text{Div } \mathbf{B} = 0 \quad \forall \omega, \omega|_{\partial B_D} = \phi$

$$\int_B [\text{GRAD } \omega] : \mathbf{B} \, dA = \int_B \text{Div}(\omega \cdot \mathbf{B}) \, dA$$

$$\int_B [\text{GRAD } \omega] : \mathbf{B} \, dA = \int_{\partial B_N} \omega \cdot \mathbf{t}_0 \, dL$$





# FROM WEAK FORM TO APPROXIMATE FORM

$$\int_B [\text{GRAD } w] : \mathbb{E} \, dA = \int_{\partial B_N} w \cdot t_0 \, dL$$

$$w^j \otimes \text{GRAD } N^j$$

$$\mathbb{E} = \mathbb{E} : \mathbb{E}$$

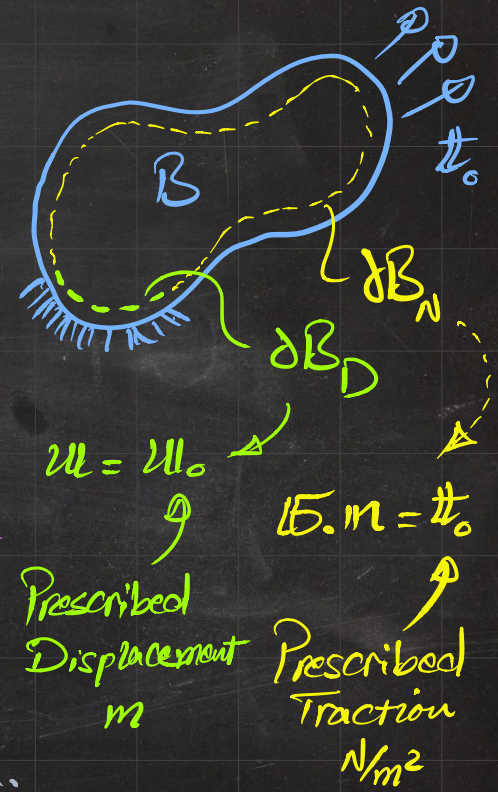
$$w = N^j w^j$$

$$\mathbb{E} = \mathbb{E} : [\text{GRAD } u]$$

$$\text{GRAD } w = w^j \otimes \text{GRAD } N^j$$

$$\text{GRAD } u = u^i \otimes \text{GRAD } N^i$$

$$u = N^i u^i = N^1 u^1 + N^2 u^2 + \dots$$



# FROM WEAK FORM TO APPROXIMATE FORM

$$\int_B [\text{GRAD } w] : \mathbb{E} \, dA = \int_{\partial B_N} w \cdot t_0 \, dL$$

$$w^j \otimes \text{GRAD } N^j$$

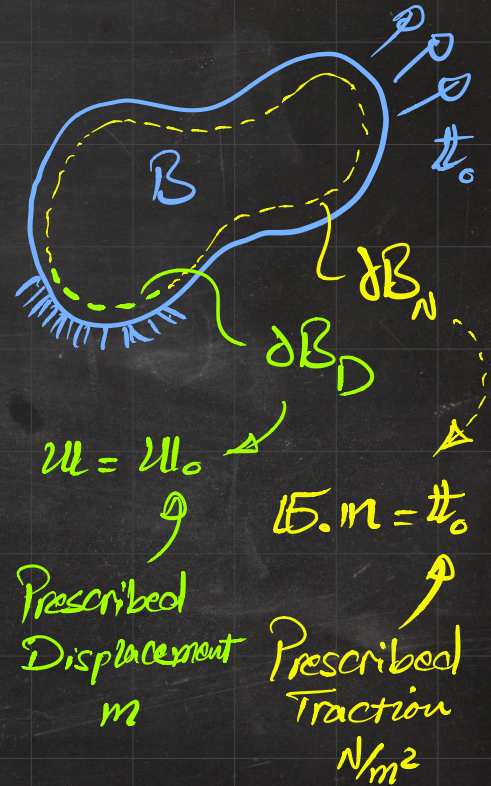
$$\mathbb{E} = \mathbb{E} : \mathbb{E}$$

$$w = N^j w^j$$

$$\mathbb{E} = \mathbb{E} : [\text{GRAD } u]$$

$$\text{GRAD } w = w^j \otimes \text{GRAD } N^j$$

$$\mathbb{E} = \mathbb{E} : [u^i \otimes \text{GRAD } N^j]$$



# FROM WEAK FORM TO APPROXIMATE FORM

$$\int_B [\text{GRAD} w] : B \, dA = \int_{\partial B_n} w \cdot t_0 \, dL$$

$$[K^{ij}]_{ac} [u^j]_c = [F^i]_a$$

$\{i, j\} \in \{1, 2, \dots, NPE\}$

$$[K^{ij}]_{ac} = \int_B [N_{12a}]_b^i E_{abcd} [N_{12a}]_d^j \, dA$$

$K^{ij}$   $\curvearrowright$  STIFFNESS BETWEEN NODES  $i$  &  $j$   
 $\hookrightarrow$   $2 \times 2$  matrix

$$[K^{ij}] = \begin{bmatrix} K_{11}^{ij} & K_{12}^{ij} \\ K_{21}^{ij} & K_{22}^{ij} \end{bmatrix}$$



## APPROXIMATE FORM

$$\left[ \mathbb{K}^{ij} \right]_{ac} \left[ u \right]_c = \left[ F^i \right]_a$$

$$\hookrightarrow \left[ \mathbb{K} \right] \left[ u \right] = \left[ F \right]$$

$\{i, j\} \in \{1, 2, \dots, NPE\}$

$$\left[ \mathbb{K}^{ij} \right]_{ac} = \int_B \left[ N_{,a}^i \right]_b E_{abcd} \left[ N_{,a}^j \right]_d dA$$

$\mathbb{K}^{ij}$   $\rightarrow$  STIFFNESS  
BETWEEN  
NODES  
 $i$  &  $j$   
 $\hookrightarrow$   $2 \times 2$   
matrix

$$\left[ \mathbb{K}^{ij} \right] = \begin{bmatrix} k_{11}^{ij} & k_{12}^{ij} \\ k_{21}^{ij} & k_{22}^{ij} \end{bmatrix}$$

UNDERSTANDING  $[K^{ij}]_{ac}$   $\rightarrow$   $K^{ij}_{ac}$   $\rightarrow$  SUPERSCRIPTS  $\rightarrow$  NODES  
 $\rightarrow$  SUBSCRIPTS  $\rightarrow$  DIRECTIONS

$$[K^{ij}]_{ac}$$

$$[K^{ij}]_{ac} = \int_B [N_{,ac}]_b^i E_{abcd} [N_{,cd}]_d^j dA$$

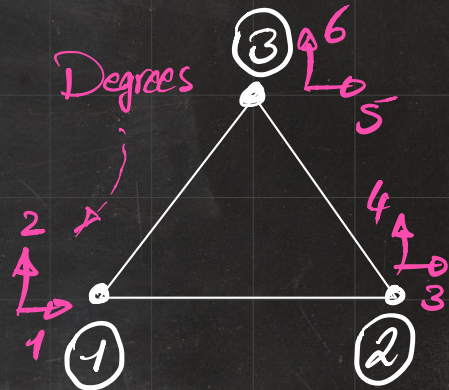
$$K^{ij}_{ac} = \frac{\delta F_a^i}{\delta u_c^j}$$

$\rightarrow$  STIFFNESS BETWEEN  
 DIRECTION  $a$  of NODE  $i$   
 &  
 DIRECTION  $c$  of NODE  $j$



$$K_{\Delta} = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$

6x6  
 ↳ Non x PD  
 ↳<sub>3</sub> ↳<sub>2</sub>

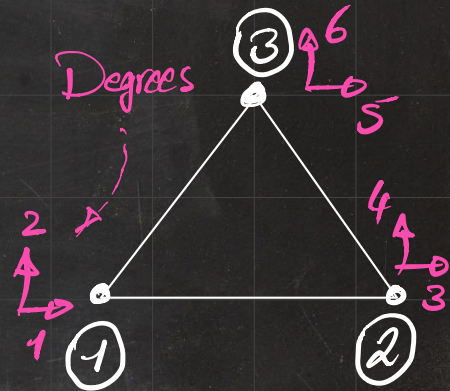


$$K_{\Delta} = \begin{bmatrix} \begin{matrix} K_{11}^{11} & K_{12}^{11} \\ K_{21}^{11} & K_{22}^{11} \end{matrix} & \begin{matrix} K_{11}^{12} & K_{12}^{12} \\ K_{21}^{12} & K_{22}^{12} \end{matrix} & \begin{matrix} K_{11}^{13} & K_{12}^{13} \\ K_{21}^{13} & K_{22}^{13} \end{matrix} \\ \begin{matrix} K_{11}^{21} & K_{12}^{21} \\ K_{21}^{21} & K_{22}^{21} \end{matrix} & \begin{matrix} K_{11}^{22} & K_{12}^{22} \\ K_{21}^{22} & K_{22}^{22} \end{matrix} & \begin{matrix} K_{11}^{23} & K_{12}^{23} \\ K_{21}^{23} & K_{22}^{23} \end{matrix} \\ \begin{matrix} K_{11}^{31} & K_{12}^{31} \\ K_{21}^{31} & K_{22}^{31} \end{matrix} & \begin{matrix} K_{11}^{32} & K_{12}^{32} \\ K_{21}^{32} & K_{22}^{32} \end{matrix} & \begin{matrix} K_{11}^{33} & K_{12}^{33} \\ K_{21}^{33} & K_{22}^{33} \end{matrix} \end{bmatrix}$$

- 1 no NODE<sup>1</sup> x
- 2 no NODE<sup>1</sup> y
- 3 no NODE<sup>2</sup> x
- 4 no NODE<sup>2</sup> y
- 5 no NODE<sup>3</sup> x
- 6 no NODE<sup>3</sup> y

$$K_{\Delta} = \begin{bmatrix} K^{11} & & & & & \\ & K^{12} & & & & \\ & & K^{13} & & & \\ & K^{21} & & K^{22} & & K^{23} \\ & & & & K^{32} & & K^{33} \\ & K^{31} & & & & & & K^{33} \end{bmatrix}$$

6x6  
Non-symmetric

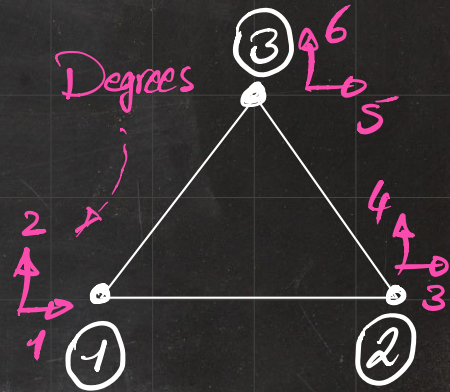


$$K_{\Delta} = \begin{bmatrix} \begin{matrix} K_{11}^{11} & K_{12}^{11} \\ K_{21}^{11} & K_{22}^{11} \end{matrix} & \begin{matrix} K_{11}^{12} & K_{12}^{12} \\ K_{21}^{12} & K_{22}^{12} \end{matrix} & \begin{matrix} K_{11}^{13} & K_{12}^{13} \\ K_{21}^{13} & K_{22}^{13} \end{matrix} & \begin{matrix} 1x \\ 1y \end{matrix} \\ \begin{matrix} K_{11}^{21} & K_{12}^{21} \\ K_{21}^{21} & K_{22}^{21} \end{matrix} & \begin{matrix} K_{11}^{22} & K_{12}^{22} \\ K_{21}^{22} & K_{22}^{22} \end{matrix} & \begin{matrix} K_{11}^{23} & K_{12}^{23} \\ K_{21}^{23} & K_{22}^{23} \end{matrix} & \begin{matrix} 2x \\ 2y \end{matrix} \\ \begin{matrix} K_{11}^{31} & K_{12}^{31} \\ K_{21}^{31} & K_{22}^{31} \end{matrix} & \begin{matrix} K_{11}^{32} & K_{12}^{32} \\ K_{21}^{32} & K_{22}^{32} \end{matrix} & \begin{matrix} K_{11}^{33} & K_{12}^{33} \\ K_{21}^{33} & K_{22}^{33} \end{matrix} & \begin{matrix} 3x \\ 3y \end{matrix} \end{bmatrix}$$

- 1 no NODE<sup>1</sup> X
- 2 no NODE<sup>1</sup> Y
- 3 no NODE<sup>2</sup> X
- 4 no NODE<sup>2</sup> Y
- 5 no NODE<sup>3</sup> X
- 6 no NODE<sup>3</sup> Y

$$K_{\Delta} = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$

6x6  
Non-symmetric PD  
↑<sub>3</sub> ↑<sub>2</sub>



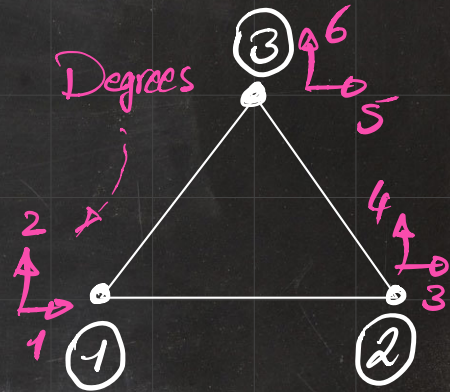
$$K_{\Delta} = \begin{bmatrix} 1_x & 1_y & 2_x & 2_y & 3_x & 3_y & 1_x \\ K_{11} & K_{12} & K_{13} & K_{14} & K_{15} & K_{16} & 1_y \\ K_{21} & K_{22} & K_{23} & K_{24} & K_{25} & K_{26} & 2_x \\ K_{31} & K_{32} & K_{33} & K_{34} & K_{35} & K_{36} & 2_y \\ K_{41} & K_{42} & K_{43} & K_{44} & K_{45} & K_{46} & 3_x \\ K_{51} & K_{52} & K_{53} & K_{54} & K_{55} & K_{56} & 3_y \\ K_{61} & K_{62} & K_{63} & K_{64} & K_{65} & K_{66} & 3_y \end{bmatrix}$$

- 1 no NODE<sup>1</sup> x
- 2 no NODE<sup>1</sup> y
- 3 no NODE<sup>2</sup> x
- 4 no NODE<sup>2</sup> y
- 5 no NODE<sup>3</sup> x
- 6 no NODE<sup>3</sup> y



$$K_{\Delta} = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$

6x6  
 ↳ NonN x PD  
 ↑<sub>3</sub> ↑<sub>2</sub>



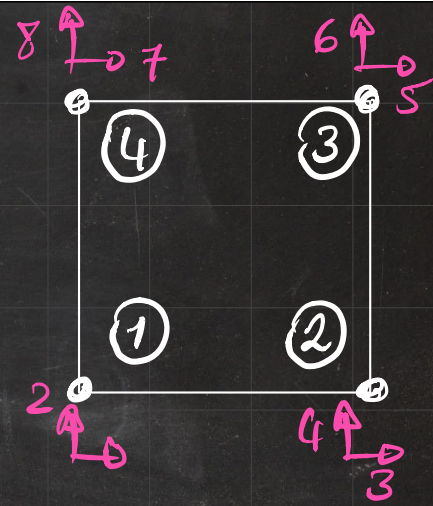
$$K_{\Delta} = \begin{bmatrix} 1_x & 1_y & 2_x & 2_y & 3_x & 3_y \\ K_{11} & K_{12} & K_{13} & K_{14} & K_{15} & K_{16} & 1_x & \text{---} & 1 \text{ no NODE } 1_x \\ K_{21} & K_{22} & K_{23} & K_{24} & K_{25} & K_{26} & 1_y & \text{---} & 2 \text{ no NODE } 1_y \\ K_{31} & K_{32} & K_{33} & K_{34} & K_{35} & K_{36} & 2_x & \text{---} & 3 \text{ no NODE } 2_x \\ K_{41} & K_{42} & K_{43} & K_{44} & K_{45} & K_{46} & 2_y & \text{---} & 4 \text{ no NODE } 2_y \\ K_{51} & K_{52} & K_{53} & K_{54} & K_{55} & K_{56} & 3_x & \text{---} & 5 \text{ no NODE } 3_x \\ K_{61} & K_{62} & K_{63} & K_{64} & K_{65} & K_{66} & 3_y & \text{---} & 6 \text{ no NODE } 3_y \end{bmatrix}$$

D2Q4u4n



$$K = \begin{bmatrix} K_{11} & K_{12} & K_{13} & K_{14} \\ K_{21} & K_{22} & K_{23} & K_{24} \\ K_{31} & K_{32} & K_{33} & K_{34} \\ K_{41} & K_{42} & K_{43} & K_{44} \end{bmatrix}$$

8x8  
 NonN x PD  
 2x4 2x2



$$K_{ij} = \begin{bmatrix} K_{11}^{ij} & K_{12}^{ij} \\ K_{21}^{ij} & K_{22}^{ij} \end{bmatrix} = \begin{bmatrix} K_{xx}^{ij} & K_{xy}^{ij} \\ K_{yx}^{ij} & K_{yy}^{ij} \end{bmatrix}$$

1, 2 - NODE<sup>1</sup><sub>xy</sub>  
 3, 4 - NODE<sup>2</sup><sub>xy</sub>  
 5, 6 - NODE<sup>3</sup><sub>xy</sub>  
 7, 8 - NODE<sup>4</sup><sub>xy</sub>



D2TR3N

$[K]_{6 \times 6}$

D2TR6N

$[K]_{12 \times 12}$

D2QU4N

$[K]_{8 \times 8}$

D2QU8N

$[K]_{8 \times 8}$

D2QU9N

$[K]_{16 \times 16}$

$[K]_{18 \times 18}$

$$[K]_{ac}^{ij} = \int_B [N]_{,ac}^i E_{abcd} [N]_{,cd}^j dA$$

## PROBLEMS TO ADDRESS

↳ INTEGRAL ↳ GAUSS QUADRATURE RULE

↳  $f(x)$  ↳  $x \rightarrow \xi$

↳  $E_{abcd}$  ↳ ?

D2TR 3N

$[K]_{6 \times 6}$

D2TR 6N

$[K]_{12 \times 12}$

D2QU 4N

$[K]_{8 \times 8}$

D2QU 8N

$[K]_{16 \times 16}$

D2QU 9N

$[K]_{18 \times 18}$

$E_{abcd} = \frac{E}{2(1+\nu)} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$

CONSTITUTIVE TENSOR

4th. O.

2x2x2x2 = 16 COMPONENTS

$+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$

Young's Modulus

$\nu$ : Poisson's Ratio

$\delta$ : Kronecker Delta

$[K]_{ac}^{ij} = \int_B [N_{,a}]_b^i E_{abcd} [N_{,a}]_d^j dA$

D2TR 3N

$$\leftarrow [K]_{6 \times 6}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

D2TR 6N

$$\leftarrow [K]_{12 \times 12}$$

$$\nu = \frac{\nu_{3D}}{1-\nu_{3D}} + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

D2QU 4N

$$\leftarrow$$

$$E_{ijkl} = \frac{E}{[1+\nu]} + \frac{E\nu}{1-\nu^2} \text{ PLANE STRAIN}$$

D2QU 8N

$$\leftarrow [K]_{8 \times 8}$$

a  
b  
c  
d

D2QU 9N

$$\leftarrow [K]_{16 \times 16}$$

$$= \frac{E[1+\nu] + E\nu}{1-\nu^2} = \frac{E}{1-\nu^2}$$

$$\leftarrow [K]_{18 \times 18}$$

$$[K]_{ac}^{ij} = \int_B [N_{,ac}]_b^i E_{abcd} [N_{,ac}]_d^j dA$$



$$[K]_{ac}^{ij} = \int_B [N_{,ac}]_b^i E_{abcd} [N_{,ac}]_d^j dA$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$E_{1111} = \frac{E}{[1-\nu^2]}$$

$$E_{1112} = 0$$

$$E_{1121} = 0$$

$$E_{1122} = \frac{E\nu}{[1-\nu^2]}$$

$$E_{1211} = 0$$

$$E_{1212} = \frac{E}{2[1+\nu]}$$

$$E_{1221} = \frac{E}{2[1+\nu]}$$

$$E_{1222} = 0$$

$$E_{2111} = 0$$

$$E_{2112} = \frac{E}{2[1+\nu]}$$

$$E_{2121} = \frac{E}{2[1+\nu]}$$

$$E_{2122} = 0$$

$$E_{2211} = \frac{E\nu}{[1-\nu^2]}$$

$$E_{2212} = 0$$

$$E_{2221} = 0$$

$$E_{2222} = \frac{E}{[1-\nu^2]}$$



$$[K]_{ac}^{ij} = \int_B [N_{,ac}^i]_b E_{abcd} [N_{,ac}^j]_d dA$$

$N_{,ac}^i$

$x = x(\xi)$

$x = x(\xi, \eta)$

$y = y(\xi, \eta)$

↳

$$\begin{bmatrix} \frac{\partial N^i}{\partial x} \\ \frac{\partial N^i}{\partial y} \end{bmatrix}$$

$$\frac{\partial N^i}{\partial x} = \frac{\partial N^i}{\partial \xi} \frac{\partial \xi}{\partial x} + \frac{\partial N^i}{\partial \eta} \frac{\partial \eta}{\partial x}$$

$$\frac{\partial N^i}{\partial y} = \frac{\partial N^i}{\partial \xi} \frac{\partial \xi}{\partial y} + \frac{\partial N^i}{\partial \eta} \frac{\partial \eta}{\partial y}$$

$\xi = \xi(x, y)$

$\eta = \eta(x, y)$

$\xi = \xi(x)$

$$N_{,\alpha}^i$$

$$[K]_{ac}^{ij} = \int_B [N_{,\alpha}^i]_b E_{abcd} [N_{,\alpha}^j]_d dA$$

$$x = x(\xi, \eta)$$

$$y = y(\xi, \eta)$$

$$x = x(\xi)$$

$$\begin{bmatrix} \frac{\partial N^i}{\partial x} \\ \frac{\partial N^i}{\partial y} \end{bmatrix} = \begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \eta}{\partial x} \\ \frac{\partial \xi}{\partial y} & \frac{\partial \eta}{\partial y} \end{bmatrix} \begin{bmatrix} \frac{\partial N^i}{\partial \xi} \\ \frac{\partial N^i}{\partial \eta} \end{bmatrix}$$

$$\underbrace{\hspace{10em}}_{N_{,\alpha}^i}$$

$$\underbrace{\hspace{10em}}_{N_{,\xi}^i}$$

$$\frac{\partial N^i}{\partial x} \leftarrow N_{,\alpha}^i$$

$$\frac{\partial N^i}{\partial \xi} \leftarrow N_{,\xi}^i$$

$$\xi = \xi(x, y)$$

$$\eta = \eta(x, y)$$

$$\xi = \xi(x)$$

$$N_{,\alpha}^i$$

$$[K]_{ac}^{ij} = \int_B [N_{,\alpha}^i]_b E_{abcd} [N_{,\alpha}^j]_d dA$$

$$x = x(\xi, \eta)$$

$$y = y(\xi, \eta)$$

$$\begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \xi}{\partial y} \\ \frac{\partial \eta}{\partial x} & \frac{\partial \eta}{\partial y} \end{bmatrix}$$

$$\frac{\partial \xi}{\partial x} \left[ \frac{\partial u}{\partial w} \right]_{\alpha\beta} = \frac{\partial u_{\alpha}}{\partial V_{\beta}}$$

$$x = x(\xi)$$

$$N_{,\alpha}^i = \begin{bmatrix} \dots \end{bmatrix} N_{,\xi}^i$$

$$\xi = \xi(x, y)$$

$$\eta = \eta(x, y)$$

$$\frac{\partial x}{\partial \xi} \begin{bmatrix} \frac{\partial x}{\partial \xi} & \frac{\partial x}{\partial \eta} \\ \frac{\partial y}{\partial \xi} & \frac{\partial y}{\partial \eta} \end{bmatrix}$$

$$\begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \eta}{\partial x} \\ \frac{\partial \xi}{\partial y} & \frac{\partial \eta}{\partial y} \end{bmatrix}$$

$$\xi = \xi(x)$$



$$N_{,\alpha}^i$$

$$[K]_{ac}^{ij} = \int_B [N_{,\alpha}^i]_b E_{abcd} [N_{,\alpha}^j]_d dA$$

$$x = x(\xi, \eta)$$

$$y = y(\xi, \eta)$$

$$x = x(\xi)$$

$$\begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \xi}{\partial y} \\ \frac{\partial \eta}{\partial x} & \frac{\partial \eta}{\partial y} \end{bmatrix}$$

$$J = \frac{\partial x}{\partial \xi}$$

$$J^{-1} = \frac{\partial \xi}{\partial x}$$

$$N_{,\alpha}^i = \begin{bmatrix} \dots \end{bmatrix} N_{,\xi}^i$$

$$\begin{bmatrix} \frac{\partial \xi}{\partial x} & \frac{\partial \eta}{\partial x} \\ \frac{\partial \xi}{\partial y} & \frac{\partial \eta}{\partial y} \end{bmatrix} = J^{-T}$$

$$\xi = \xi(x, y)$$

$$\eta = \eta(x, y)$$

$$\xi = \xi(x)$$



$$[K]_{ac}^{ij} = \int_B [N_{,ac}]_b^i E_{abcd} [N_{,cd}]_d^j dA$$

$$[K]_{ac}^{ij} = \int_B [\mathbb{J} \cdot N_{,\xi}^i]_b^{-t} E_{abcd} [\mathbb{J} \cdot N_{,\xi}^j]_d^{-t} dA$$

$$\mathbb{J} = \frac{\partial x}{\partial \xi} \quad \hookrightarrow x = x(\xi) \quad \nearrow \quad x = N^s \xi^s$$

$$\hookrightarrow N^s(\xi, \eta)$$

$$[K]_{ac}^{ij} = \int_B [\mathcal{J} \cdot N_{,a}^i]_b E_{abcd} [\mathcal{J} \cdot N_{,c}^j]_d dA$$

$$J_{11} = \frac{\partial x}{\partial \xi} = x^1 \frac{\partial N^1}{\partial \xi} + x^2 \frac{\partial N^2}{\partial \xi} + \dots + x^{NPE} \frac{\partial N^{NPE}}{\partial \xi}$$

$$J_{12} = \frac{\partial x}{\partial \eta} = x^1 \frac{\partial N^1}{\partial \eta} + x^2 \frac{\partial N^2}{\partial \eta} + \dots + x^{NPE} \frac{\partial N^{NPE}}{\partial \eta}$$

$$J_{21} = \frac{\partial y}{\partial \xi} = y^1 \frac{\partial N^1}{\partial \xi} + y^2 \frac{\partial N^2}{\partial \xi} + \dots + y^{NPE} \frac{\partial N^{NPE}}{\partial \xi}$$

$$J_{22} = \frac{\partial y}{\partial \eta} = y^1 \frac{\partial N^1}{\partial \eta} + y^2 \frac{\partial N^2}{\partial \eta} + \dots + y^{NPE} \frac{\partial N^{NPE}}{\partial \eta}$$

$$[K]_{ac}^{ij} = \int_B [\mathcal{J} \cdot N_{,a}^i]_b E_{abcd} [\mathcal{J} \cdot N_{,c}^j]_d dA$$

$$\underbrace{\begin{bmatrix} \mathcal{J}_{11} & \mathcal{J}_{21} \\ \mathcal{J}_{12} & \mathcal{J}_{22} \end{bmatrix}}_{\mathcal{J}^t} = \begin{bmatrix} \frac{\partial N^1}{\partial \xi} & \frac{\partial N^2}{\partial \xi} & \dots & \frac{\partial N^{NPE}}{\partial \xi} \\ \frac{\partial N^1}{\partial \eta} & \frac{\partial N^2}{\partial \eta} & \dots & \frac{\partial N^{NPE}}{\partial \eta} \end{bmatrix} \begin{bmatrix} \alpha^1 & y^1 \\ \alpha^2 & y^2 \\ \vdots & \vdots \\ \alpha^{NPE} & y^{NPE} \end{bmatrix}$$

$2 \times NPE$ 
 $NPE \times 2$



$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^T \cdot N_{,\xi}^i]_b E_{abcd} [J^T \cdot N_{,\xi}^j]_d \text{Det } J \times \alpha_{gp} \times \frac{1}{2}$$

JACOBIAN  $\frac{\partial x}{\partial \xi}$   $\rightarrow$   $J = \begin{bmatrix} x^1 \dots x^{NPE} \\ y^1 \dots y^{NPE} \end{bmatrix} \begin{bmatrix} N_{,\xi}^1 & N_{,\eta}^1 \\ \vdots & \vdots \\ N_{,\xi}^{NPE} & N_{,\eta}^{NPE} \end{bmatrix}$  IF TRIANGLE

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$\left\{ \begin{array}{llll} E_{1111} = \frac{E}{[1-\nu^2]} & E_{1112} = 0 & E_{1121} = 0 & E_{1122} = \frac{E\nu}{[1-\nu^2]} \\ E_{1211} = 0 & E_{1212} = \frac{E}{2[1+\nu]} & E_{1221} = \frac{E}{2[1+\nu]} & E_{1222} = 0 \\ E_{2111} = 0 & E_{2112} = \frac{E}{2[1+\nu]} & E_{2121} = \frac{E}{2[1+\nu]} & E_{2122} = 0 \\ E_{2211} = \frac{E\nu}{[1-\nu^2]} & E_{2212} = 0 & E_{2221} = 0 & E_{2222} = \frac{E}{[1-\nu^2]} \end{array} \right.$$

# FINITE ELEMENT METHOD

FINITE ELEMENT METHOD

## 2D FEM

formulation summary  
& understanding via examples

$K_{ac}^{ij}$ 

stiffness between  
direction "a" of node "i" &  
direction "c" of node "j"

$$\equiv \frac{\delta F_a^i}{\delta u_c^j}$$

## Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp}$$

## Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$



## Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{\text{GPE}} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp}$$

## Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{\text{GPE}} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1 + \nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E \nu}{1 - \nu^2} \delta_{ab} \delta_{cd}$$

## Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{\text{GPE}} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp}$$

## Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{\text{GPE}} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd} \quad \text{2D plane strain}$$

## 2D plane strain constitutive tensor components

$$E_{abcd} = \frac{E}{2[1 + \nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E \nu}{1 - \nu^2} \delta_{ab} \delta_{cd}$$

$$E_{1111} = \frac{E}{1 - \nu^2} \quad E_{1112} = 0 \quad E_{1121} = 0 \quad E_{1122} = \frac{E \nu}{1 - \nu^2}$$

$$E_{1211} = 0 \quad E_{1212} = \frac{E}{2[1 + \nu]} \quad E_{1221} = \frac{E}{2[1 + \nu]} \quad E_{1222} = 0$$

$$E_{2111} = 0 \quad E_{2112} = \frac{E}{2[1 + \nu]} \quad E_{2121} = \frac{E}{2[1 + \nu]} \quad E_{2122} = 0$$

$$E_{2211} = \frac{E \nu}{1 - \nu^2} \quad E_{2212} = 0 \quad E_{2221} = 0 \quad E_{2222} = \frac{E}{1 - \nu^2}$$



$K_{ac}^{ij}$  stiffness between direction "a" of node "i" & direction "c" of node "j"

Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp} \times \frac{1}{2}$$

$$J = \frac{\partial x}{\partial \xi} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix}$$

$$\begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$K_{ac}^{ij}$  stiffness between  
direction "a" of node "i" &  
direction "c" of node "j"

**Quadrilateral Elements**

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp}$$

**Triangular Elements**

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \xi} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

plane strain  $+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$

$$K_{ac}^{ij}$$

stiffness between  
direction "a" of node "i" &  
direction "c" of node "j"

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp}$$

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

plane strain

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

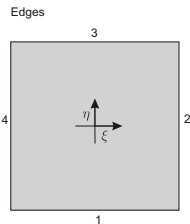
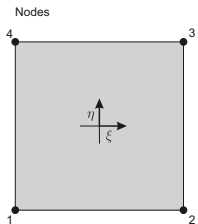
$$\begin{aligned} E_{1111} &= \frac{E}{1-\nu^2} & E_{1112} &= 0 & E_{1121} &= 0 & E_{1122} &= \frac{E\nu}{1-\nu^2} \\ E_{1211} &= 0 & E_{1212} &= \frac{E}{2[1+\nu]} & E_{1221} &= \frac{E}{2[1+\nu]} & E_{1222} &= 0 \\ E_{2111} &= 0 & E_{2112} &= \frac{E}{2[1+\nu]} & E_{2121} &= \frac{E}{2[1+\nu]} & E_{2122} &= 0 \\ E_{2211} &= \frac{E\nu}{1-\nu^2} & E_{2212} &= 0 & E_{2221} &= 0 & E_{2222} &= \frac{E}{1-\nu^2} \end{aligned}$$



- two-dimensional 4-noded quadrilateral element (D2QU4N)  
a.k.a. bilinear quadrilateral element
- two-dimensional 9-noded quadrilateral element (D2QU9N)  
a.k.a. Lagrange biquadratic quadrilateral element
- two-dimensional 8-noded quadrilateral element (D2QU8N)  
a.k.a. serendipity biquadratic quadrilateral element
- two-dimensional 3-noded triangular element (D2TR3N)  
a.k.a. constant strain triangle
- two-dimensional 6-noded triangular element (D2TR6N)  
a.k.a. quadratic triangle
- two-dimensional quadrature rule

## D2QU4N

## bilinear quadrilateral element



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1

$$N^1 = \frac{1}{4} (1 - \xi) (1 - \eta)$$

$$N^2 = \frac{1}{4} (1 + \xi) (1 - \eta)$$

$$N^3 = \frac{1}{4} (1 + \xi) (1 + \eta)$$

$$N^4 = \frac{1}{4} (1 - \xi) (1 + \eta)$$

$$N_{,\xi}^1 = -\frac{1}{4} (1 - \eta)$$

$$N_{,\xi}^2 = +\frac{1}{4} (1 - \eta)$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + \eta)$$

$$N_{,\xi}^4 = -\frac{1}{4} (1 + \eta)$$

$$N_{,\eta}^1 = -\frac{1}{4} (1 - \xi)$$

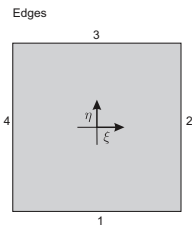
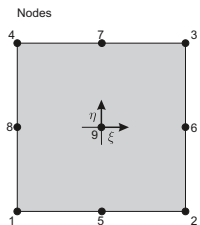
$$N_{,\eta}^2 = -\frac{1}{4} (1 + \xi)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi)$$

$$N_{,\eta}^4 = +\frac{1}{4} (1 - \xi)$$

## D2QU9N

## Lagrange biquadratic quadrilateral element



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1
5	0	-1
6	1	0
7	0	1
8	-1	0
9	0	0

$$N^1 = +\frac{1}{4} (1 - \xi) \xi (1 - \eta) \eta$$

$$N^2 = -\frac{1}{4} (1 + \xi) \xi (1 - \eta) \eta$$

$$N^3 = +\frac{1}{4} (1 + \xi) \xi (1 + \eta) \eta$$

$$N^4 = -\frac{1}{4} (1 - \xi) \xi (1 + \eta) \eta$$

$$N^5 = -\frac{1}{2} (1 - \xi) (1 + \xi) (1 - \eta) \eta$$

$$N^6 = +\frac{1}{2} (1 + \xi) \xi (1 - \eta) (1 + \eta)$$

$$N^7 = +\frac{1}{2} (1 - \xi) (1 + \xi) (1 + \eta) \eta$$

$$N^8 = -\frac{1}{2} (1 - \xi) \xi (1 - \eta) (1 + \eta)$$

$$N^9 = (1 - \xi) (1 + \xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^1 = +\frac{1}{4} (1 - 2\xi) (1 - \eta) \eta$$

$$N_{,\xi}^2 = -\frac{1}{4} (1 + 2\xi) (1 - \eta) \eta$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + 2\xi) (1 + \eta) \eta$$

$$N_{,\xi}^4 = -\frac{1}{4} (1 - 2\xi) (1 + \eta) \eta$$

$$N_{,\xi}^5 = \xi \eta (1 - \eta)$$

$$N_{,\xi}^6 = \frac{1}{2} (1 + 2\xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^7 = -\xi \eta (1 + \eta)$$

$$N_{,\xi}^8 = -\frac{1}{2} (1 - 2\xi) (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^9 = -2\xi (1 - \eta) (1 + \eta)$$

$$N_{,\eta}^1 = +\frac{1}{4} (1 - \xi) \xi (1 - 2\eta)$$

$$N_{,\eta}^2 = -\frac{1}{4} (1 + \xi) \xi (1 - 2\eta)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi) \xi (1 + 2\eta)$$

$$N_{,\eta}^4 = -\frac{1}{4} (1 - \xi) \xi (1 + 2\eta)$$

$$N_{,\eta}^5 = \frac{1}{2} (1 - \xi) (1 + \xi) (2\eta - 1)$$

$$N_{,\eta}^6 = -(1 + \xi) \xi \eta$$

$$N_{,\eta}^7 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 + 2\eta)$$

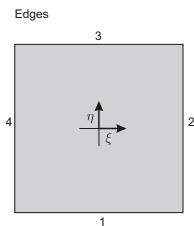
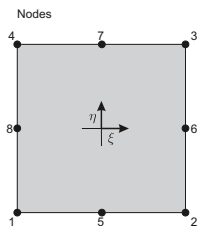
$$N_{,\eta}^8 = (1 - \xi) \xi \eta$$

$$N_{,\eta}^9 = -2(1 - \xi) (1 + \xi) \eta$$



## D2QU8N

## serendipity biquadratic quadrilateral element



Node Number	Coordinates	
	$\xi$	$\eta$
1	-1	-1
2	1	-1
3	1	1
4	-1	1
5	0	-1
6	1	0
7	0	1
8	-1	0

$$N^1 = -\frac{1}{4} (1 - \xi) (1 - \eta) (1 + \xi + \eta)$$

$$N^2 = -\frac{1}{4} (1 + \xi) (1 - \eta) (1 - \xi + \eta)$$

$$N^3 = -\frac{1}{4} (1 + \xi) (1 + \eta) (1 - \xi - \eta)$$

$$N^4 = -\frac{1}{4} (1 - \xi) (1 + \eta) (1 + \xi - \eta)$$

$$N^5 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 - \eta)$$

$$N^6 = \frac{1}{2} (1 + \xi) (1 + \eta) (1 - \eta)$$

$$N^7 = \frac{1}{2} (1 - \xi) (1 + \xi) (1 + \eta)$$

$$N^8 = \frac{1}{2} (1 - \xi) (1 + \eta) (1 - \eta)$$

$$N_{,\xi}^1 = +\frac{1}{4} (1 - \eta) (2\xi + \eta)$$

$$N_{,\xi}^2 = +\frac{1}{4} (1 - \eta) (2\xi - \eta)$$

$$N_{,\xi}^3 = +\frac{1}{4} (1 + \eta) (2\xi + \eta)$$

$$N_{,\xi}^4 = +\frac{1}{4} (1 + \eta) (2\xi - \eta)$$

$$N_{,\xi}^5 = -\xi (1 - \eta)$$

$$N_{,\xi}^6 = +\frac{1}{2} (1 - \eta) (1 + \eta)$$

$$N_{,\xi}^7 = -\xi (1 + \eta)$$

$$N_{,\xi}^8 = -\frac{1}{2} (1 - \eta) (1 + \eta)$$

$$N_{,\eta}^1 = +\frac{1}{4} (1 - \xi) (\xi + 2\eta)$$

$$N_{,\eta}^2 = +\frac{1}{4} (1 + \xi) (-\xi + 2\eta)$$

$$N_{,\eta}^3 = +\frac{1}{4} (1 + \xi) (\xi + 2\eta)$$

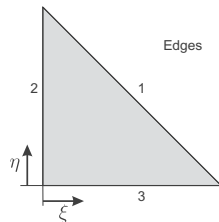
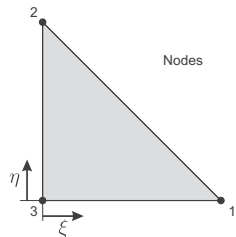
$$N_{,\eta}^4 = +\frac{1}{4} (1 - \xi) (-\xi + 2\eta)$$

$$N_{,\eta}^5 = -\frac{1}{2} (1 - \xi) (1 + \xi)$$

$$N_{,\eta}^6 = -(1 + \xi) \eta$$

$$N_{,\eta}^7 = +\frac{1}{2} (1 - \xi) (1 + \xi)$$

$$N_{,\eta}^8 = -(1 - \xi) \eta$$



Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$$N^1 = \xi$$

$$N^2 = \eta$$

$$N^3 = (1 - \xi - \eta)$$

$$N_{,\xi}^1 = 1$$

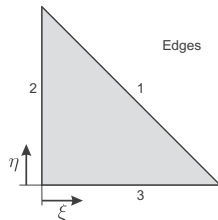
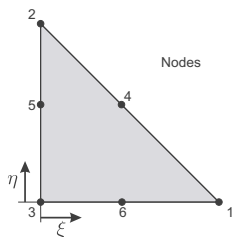
$$N_{,\xi}^2 = 0$$

$$N_{,\xi}^3 = -1$$

$$N_{,\eta}^1 = 0$$

$$N_{,\eta}^2 = 1$$

$$N_{,\eta}^3(\xi, \eta) = -1$$



Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0
4	1/2	1/2
5	0	1/2
6	1/2	0

$$N^1 = \xi(2\xi - 1)$$

$$N^1_{,\xi} = -1 + 4\xi$$

$$N^1_{,\eta} = 0$$

$$N^2 = \eta(2\eta - 1)$$

$$N^2_{,\xi} = 0$$

$$N^2_{,\eta} = -1 + 4\eta$$

$$N^3 = (1 - \xi - \eta)(1 - 2\xi - 2\eta)$$

$$N^3_{,\xi} = -3 + 4\xi + 4\eta$$

$$N^3_{,\eta} = -3 + 4\xi + 4\eta$$

$$N^4 = 4\xi\eta$$

$$N^4_{,\xi} = 4\eta$$

$$N^4_{,\eta} = 4\xi$$

$$N^5 = 4\eta(1 - \xi - \eta)$$

$$N^5_{,\xi} = -4\eta$$

$$N^5_{,\eta} = -4(-1 + 2\eta + \xi)$$

$$N^6 = 4\xi(1 - \xi - \eta)$$

$$N^6_{,\xi} = -4(-1 + \eta + 2\xi)$$

$$N^6_{,\eta} = -4\xi$$



## two-dimensional quadrature rule i

### Triangular Elements Gauss Point Rule

$$\int_0^1 \int_0^{1-\eta} \{\bullet\} d\xi d\eta \approx \frac{1}{2} \sum_{i=1}^{N_{\text{Gauss Points}}} \alpha_i \{\bullet\}_{\text{Gauss Point}^i}$$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/3	1/3	1

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/6	1/6	1/3
2	4/6	1/6	1/3
3	1/6	4/6	1/3

## two-dimensional quadrature rule ii

### Quadrilateral Elements Gauss Point Rule

$$\int_{-1}^1 \int_{-1}^1 \{\bullet\} d\xi d\eta \approx \sum_{i=1}^{N_{\text{Gauss Points}}} \alpha_i \{\bullet\}_{\text{Gauss Point}^i}$$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	0	0	$2 \times 2$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	$-1/\sqrt{3}$	$-1/\sqrt{3}$	$1 \times 1$
2	$+1/\sqrt{3}$	$-1/\sqrt{3}$	$1 \times 1$
3	$+1/\sqrt{3}$	$+1/\sqrt{3}$	$1 \times 1$
4	$-1/\sqrt{3}$	$+1/\sqrt{3}$	$1 \times 1$

## two-dimensional quadrature rule iii

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	$-\sqrt{3/5}$	$-\sqrt{3/5}$	$5/9 \times 5/9$
2	$+\sqrt{3/5}$	$-\sqrt{3/5}$	$5/9 \times 5/9$
3	$\sqrt{3/5}$	$\sqrt{3/5}$	$5/9 \times 5/9$
4	$-\sqrt{3/5}$	$\sqrt{3/5}$	$5/9 \times 5/9$
5	0	$-\sqrt{3/5}$	$5/9 \times 8/9$
6	$+\sqrt{3/5}$	0	$5/9 \times 8/9$
7	0	$\sqrt{3/5}$	$5/9 \times 8/9$
8	$-\sqrt{3/5}$	0	$5/9 \times 8/9$
9	0	0	$8/9 \times 8/9$

## Understanding Jacobian

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \xi}$$



## Understanding Jacobian


$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \xi}$$

$$d\mathbf{x} = \mathbf{J} d\xi$$

## Understanding Jacobian

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}}$$

linear mapping  
from natural space  
to physical space




$$d\mathbf{x} = \mathbf{J} d\boldsymbol{\xi}$$

## Understanding Jacobian

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

linear mapping  
from natural space  
to physical space




$$d\mathbf{x} = \mathbf{J} d\boldsymbol{\xi}$$



## Understanding Jacobian

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

linear mapping  
from natural space  
to physical space




$$d\mathbf{x} = \mathbf{J} d\boldsymbol{\xi} \quad J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$



## Understanding Jacobian

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

linear mapping  
from natural space  
to physical space

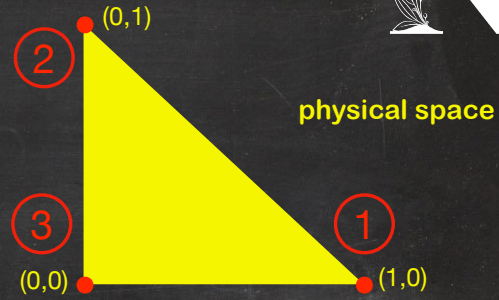


$$d\mathbf{x} = \mathbf{J} d\boldsymbol{\xi} \quad J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

often, the (scalar) determinant  
of the Jacobian matrix is also  
referred to as Jacobian

...  
the scalar Jacobian is a linear  
mapping between the area  
elements from the natural  
space to the physical space

## Example (D2TR3N) ... constant strain triangle



pay attention to numbering of the nodes !

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

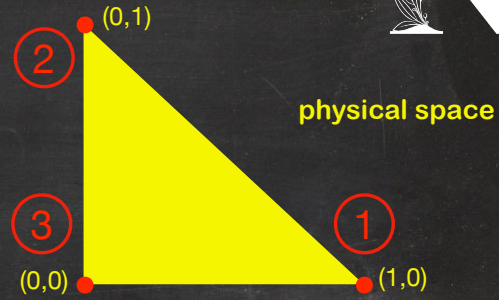
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ -1 & -1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

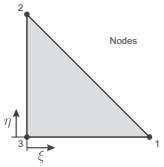


pay attention to  
numbering of  
the nodes  
!

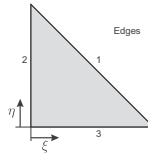
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

**natural space**



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

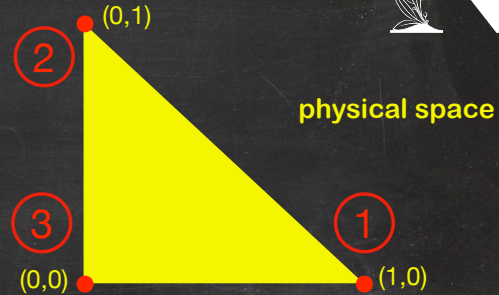
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ -1 & -1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi} = 1$$

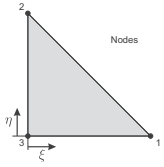
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_\xi^1 & N_\eta^1 \\ N_\xi^2 & N_\eta^2 \\ \vdots & \vdots \\ N_\xi^{\text{NPE}} & N_\eta^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi}$$

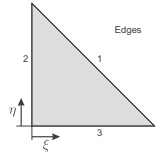


pay attention to  
numbering of  
the nodes  
!

**natural space**



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

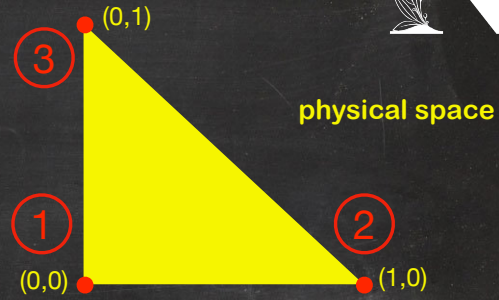
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$



# Example (D2TR3N) ... constant strain triangle



pay attention to numbering of the nodes !

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

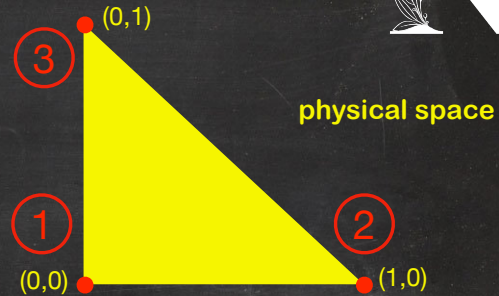
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix}$$

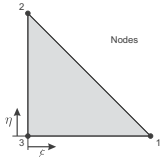


pay attention to  
numbering of  
the nodes  
!

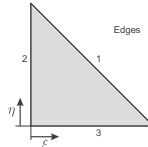
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

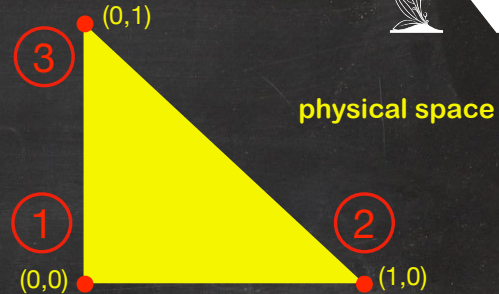
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi} = 1$$

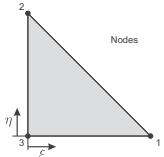
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_\xi^1 & N_\eta^1 \\ N_\xi^2 & N_\eta^2 \\ \vdots & \vdots \\ N_\xi^{\text{NPE}} & N_\eta^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi}$$

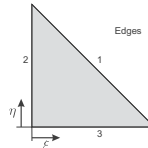


pay attention to  
numbering of  
the nodes  
!

**natural space**



Nodes



Edges

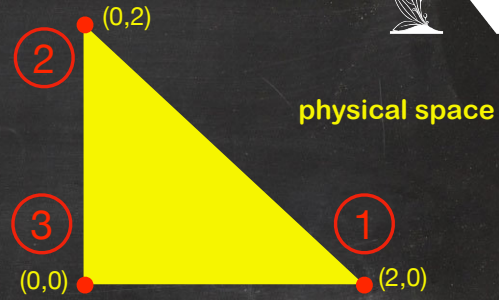
Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle



pay attention to numbering of the nodes !

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

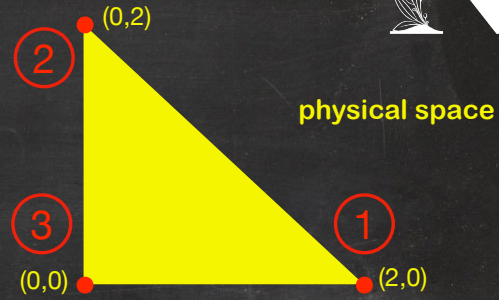
$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$



## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 2 & 0 & 0 \\ 0 & 2 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix}$$

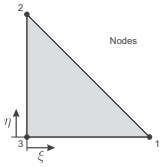


pay attention to numbering of the nodes !

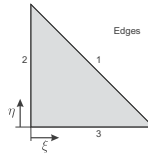
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

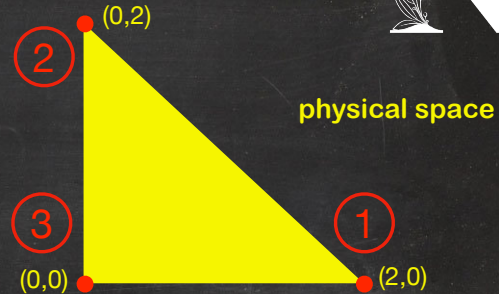
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 2 & 0 & 0 \\ 0 & 2 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 2 & 0 \\ 0 & 2 \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}} = 4$$

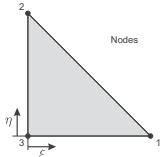
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

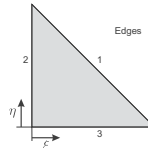


pay attention to  
numbering of  
the nodes  
!

**natural space**



Nodes



Edges

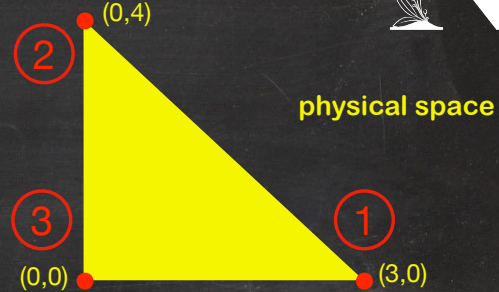
Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle



pay attention to  
numbering of  
the nodes  
!

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

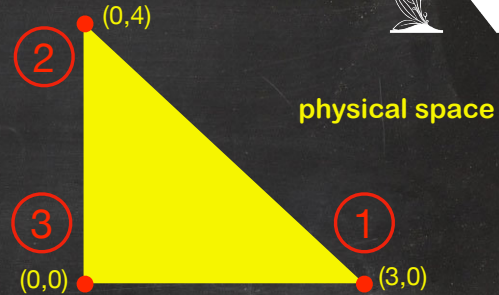
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 3 & 0 & 0 \\ 0 & 4 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 3 & 0 \\ 0 & 4 \end{bmatrix}$$

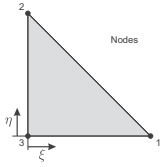


pay attention to  
numbering of  
the nodes  
!

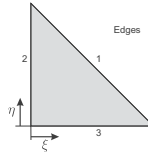
$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$



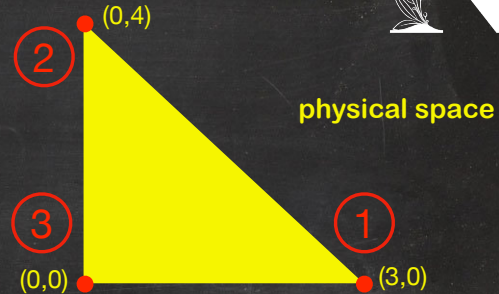
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 3 & 0 & 0 \\ 0 & 4 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 3 & 0 \\ 0 & 4 \end{bmatrix}$$

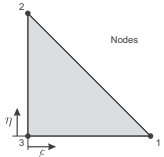
$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi} = 12$$

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_\xi^1 & N_\eta^1 \\ N_\xi^2 & N_\eta^2 \\ \vdots & \vdots \\ N_\xi^{\text{NPE}} & N_\eta^{\text{NPE}} \end{bmatrix}$$

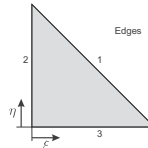
$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi}$$



natural space



Nodes



Edges

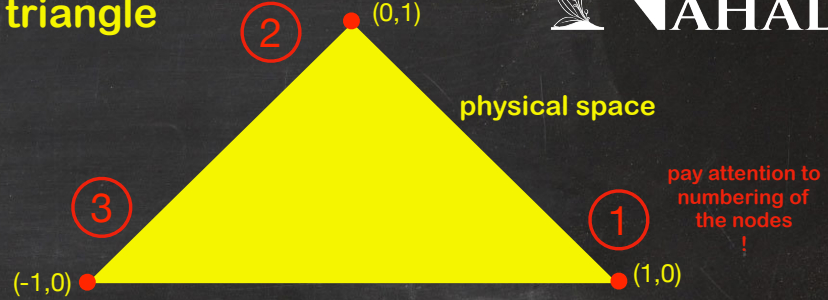
Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle



$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

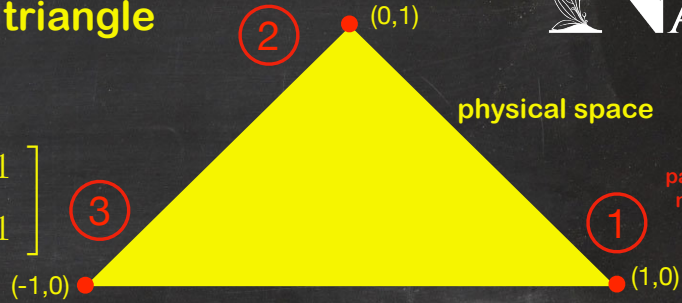
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 2 & 1 \\ 0 & 1 \end{bmatrix}$$



$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

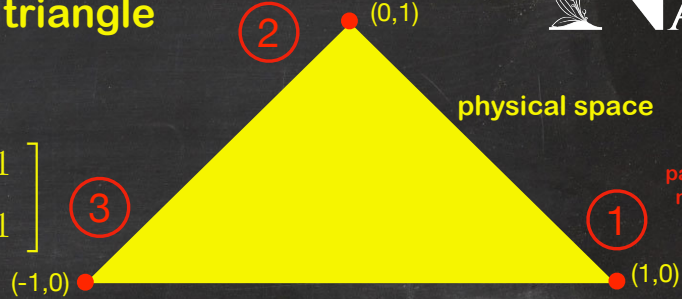
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 2 & 1 \\ 0 & 1 \end{bmatrix}$$

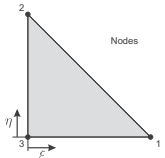
$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi} = 2$$

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_\xi^1 & N_\eta^1 \\ N_\xi^2 & N_\eta^2 \\ \vdots & \vdots \\ N_\xi^{\text{NPE}} & N_\eta^{\text{NPE}} \end{bmatrix}$$

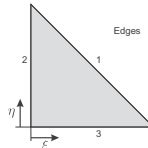
$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi}$$



natural space



Nodes



Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

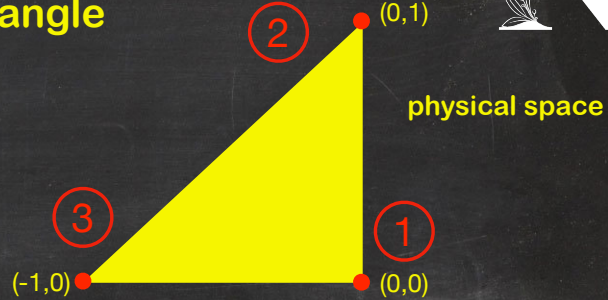
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$



# Example (D2TR3N) ... constant strain triangle



$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

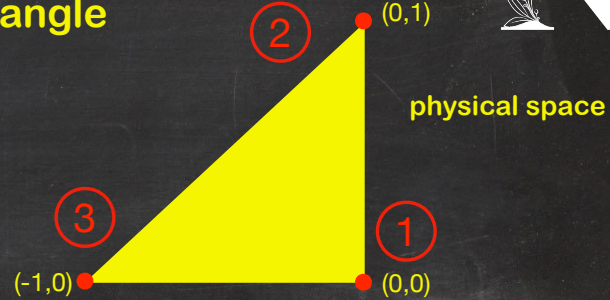
$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$



pay attention to numbering of the nodes !

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_{\mathbf{x}}}{dA_{\boldsymbol{\xi}}}$$

natural space

Nodes

Edges

Node Number	Coordinates	
	$\xi$	$\eta$
1	1	0
2	0	1
3	0	0

$N^1 = \xi$   
 $N^2 = \eta$   
 $N^3 = (1 - \xi - \eta)$

$N_{,\xi}^1 = 1$   
 $N_{,\xi}^2 = 0$   
 $N_{,\xi}^3 = -1$

$N_{,\eta}^1 = 0$   
 $N_{,\eta}^2 = 1$   
 $N_{,\eta}^3(\xi, \eta) = -1$

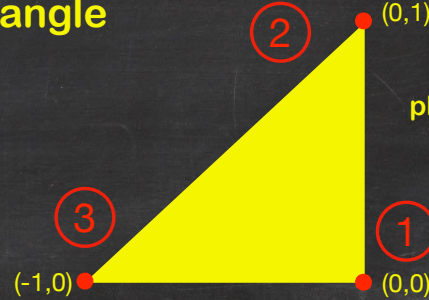
## Example (D2TR3N) ... constant strain triangle

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} 0 & 0 & -1 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$

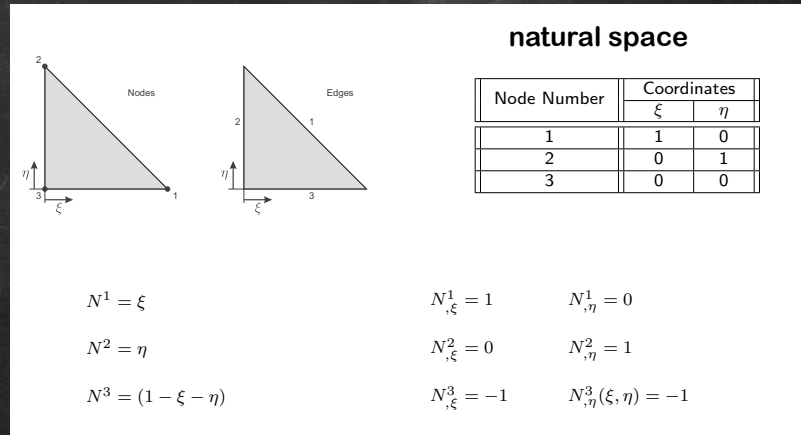
$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi} = 1$$

$$\mathbf{J} = \frac{\partial \mathbf{x}}{\partial \boldsymbol{\xi}} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_\xi^1 & N_\eta^1 \\ N_\xi^2 & N_\eta^2 \\ \vdots & \vdots \\ N_\xi^{\text{NPE}} & N_\eta^{\text{NPE}} \end{bmatrix}$$

$$J = \text{Det} \mathbf{J} = \frac{dA_x}{dA_\xi}$$



pay attention to  
numbering of  
the nodes  
!



## Example (D2TR3N) ... constant strain triangle ... stiffness

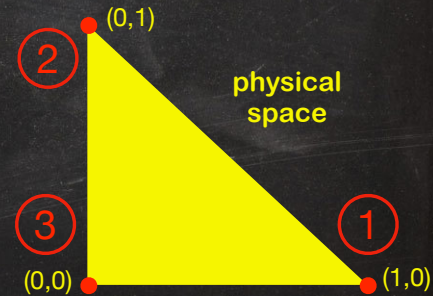
Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$





## Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

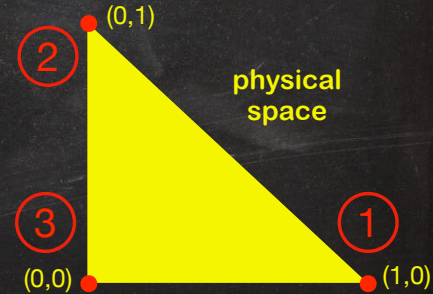
$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{K} = \begin{bmatrix} \mathbf{K}^{11} & \mathbf{K}^{12} & \mathbf{K}^{13} \\ \mathbf{K}^{21} & \mathbf{K}^{22} & \mathbf{K}^{23} \\ \mathbf{K}^{31} & \mathbf{K}^{32} & \mathbf{K}^{33} \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$



# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

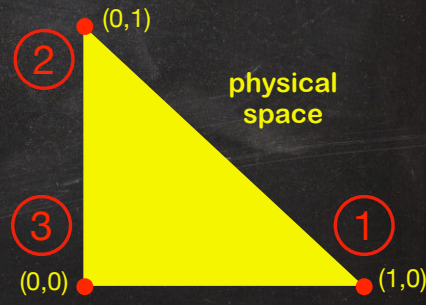
$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix} = \begin{bmatrix} K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\ K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\ K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\ K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\ K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\ K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$



# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

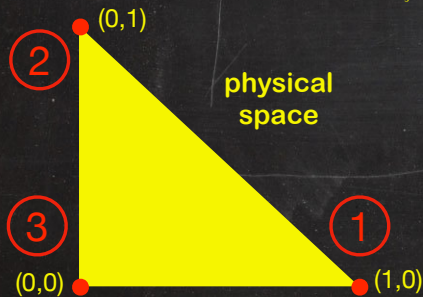
$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$



$N^1 = \xi$	<b>natural space</b>	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$		$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$		$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$$\mathbf{K} = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$



## Example (D2TR3N) ... constant strain triangle ... stiffness

in this particular case, the coordinates of the Gauss points do not enter the calculations, since the derivatives of the shape functions are constant over the element ... however, this is usually not the case and particularly holds for constant strain triangle (CST) ... also, in this case we have only one Gauss point that makes the calculations more straightforward ... otherwise the summation over the Gauss points must be carefully taken into account ...

$$\int_0^1 \int_0^{1-\eta} \{\bullet\} d\xi d\eta \approx \frac{1}{2} \sum_{i=1}^{N_{\text{Gauss Points}}} \alpha_i \{\bullet\}_{\text{Gauss Point } i}$$

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/3	1/3	1

Gauss Point Number	Coordinates		Weight Factor
	$\xi$	$\eta$	$\alpha$
1	1/6	1/6	1/3
2	4/6	1/6	1/3
3	1/6	4/6	1/3



**natural space**

$$\begin{aligned}
 N^1 &= \xi & N^1_{,\xi} &= 1 & N^1_{,\eta} &= 0 \\
 N^2 &= \eta & N^2_{,\xi} &= 0 & N^2_{,\eta} &= 1 \\
 N^3 &= (1 - \xi - \eta) & N^3_{,\xi} &= -1 & N^3_{,\eta}(\xi, \eta) &= -1
 \end{aligned}$$

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$



# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$J = \frac{\partial \mathbf{x}}{\partial \xi} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & 1 \\ -1 & -1 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$$

$$J = \text{Det}J = \frac{dA_x}{dA_\xi} = 1$$

$$E_{1111} = \frac{E}{1-\nu^2}$$

$$E_{1112} = 0$$

$$E_{1121} = 0$$

$$E_{1122} = \frac{E\nu}{1-\nu^2}$$

$$E_{1211} = 0$$

$$E_{1212} = \frac{E}{2[1+\nu]}$$

$$E_{1221} = \frac{E}{2[1+\nu]}$$

$$E_{1222} = 0$$

$$E_{2111} = 0$$

$$E_{2112} = \frac{E}{2[1+\nu]}$$

$$E_{2121} = \frac{E}{2[1+\nu]}$$

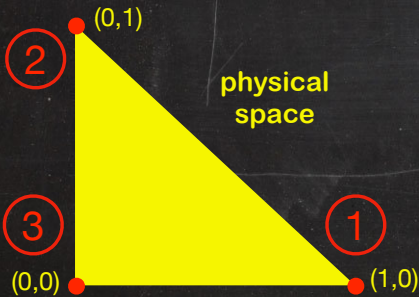
$$E_{2122} = 0$$

$$E_{2211} = \frac{E\nu}{1-\nu^2}$$

$$E_{2212} = 0$$

$$E_{2221} = 0$$

$$E_{2222} = \frac{E}{1-\nu^2}$$



$$N^1 = \xi$$

natural space

$$N_{,\xi}^1 = 1$$

$$N_{,\eta}^1 = 0$$

$$N^2 = \eta$$

$$N_{,\xi}^2 = 0$$

$$N_{,\eta}^2 = 1$$

$$N^3 = (1 - \xi - \eta)$$

$$N_{,\xi}^3 = -1$$

$$N_{,\eta}^3(\xi, \eta) = -1$$

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$

# Example (D2TR3N) ... constant strain triangle ... stiffness

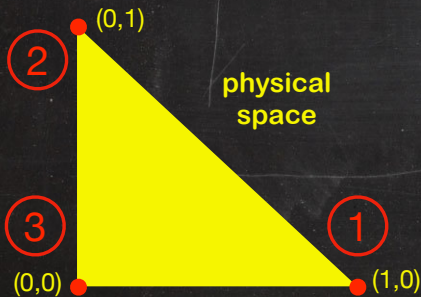
Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$



$N^1 = \xi$	<b>natural space</b>	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$		$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$		$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$

# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

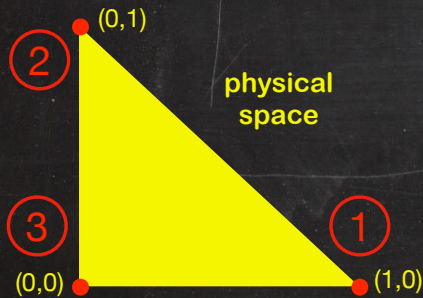
$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$K_{ac}^{ij} = [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$



$N^1 = \xi$	<b>natural space</b>	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$		$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$		$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$



# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

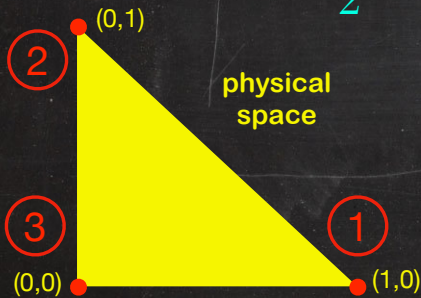
$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K_{ac}^{ij} = [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d \alpha_{gp} \times \frac{1}{2}$$

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$



$N^1 = \xi$	<b>natural space</b>	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$		$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$		$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix}$$



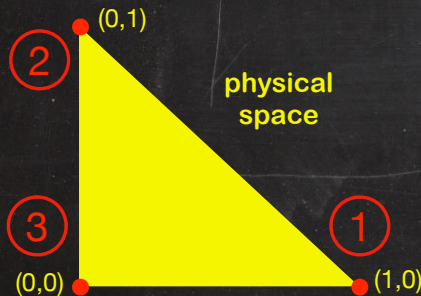
## Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N^i]_b E_{abcd} [N^j]_d$$

$$\begin{aligned}
 E_{1111} &= \frac{E}{1-\nu^2} & E_{1112} &= 0 & E_{1121} &= 0 & E_{1122} &= \frac{E\nu}{1-\nu^2} \\
 E_{1211} &= 0 & E_{1212} &= \frac{E}{2[1+\nu]} & E_{1221} &= \frac{E}{2[1+\nu]} & E_{1222} &= 0 \\
 E_{2111} &= 0 & E_{2112} &= \frac{E}{2[1+\nu]} & E_{2121} &= \frac{E}{2[1+\nu]} & E_{2122} &= 0 \\
 E_{2211} &= \frac{E\nu}{1-\nu^2} & E_{2212} &= 0 & E_{2221} &= 0 & E_{2222} &= \frac{E}{1-\nu^2}
 \end{aligned}$$

$K =$

$$\begin{bmatrix}
 K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\
 K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\
 K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\
 K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\
 K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\
 K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33}
 \end{bmatrix}$$



$N^1 = \xi$	<b>natural space</b>	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$		$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$		$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$$K = \begin{bmatrix}
 K^{11} & K^{12} & K^{13} \\
 K^{21} & K^{22} & K^{23} \\
 K^{31} & K^{32} & K^{33}
 \end{bmatrix}$$

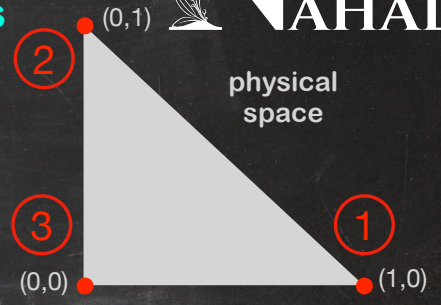
# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N^i]_{,\xi}^b E_{abcd} [N^j]_{,\xi}^d$$

$$K_{11} = \frac{1}{2} [N^1]_{,\xi}^b E_{1b1d} [N^1]_{,\xi}^d$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$

PD PD



$N^1 = \xi$	$N^1_{,\xi} = 1$	$N^1_{,\eta} = 0$
$N^2 = \eta$	$N^2_{,\xi} = 0$	$N^2_{,\eta} = 1$
$N^3 = (1 - \xi - \eta)$	$N^3_{,\xi} = -1$	$N^3_{,\eta}(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

# Example (D2TR3N) ... constant strain triangle ... stiffness

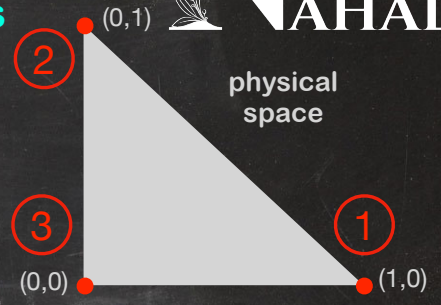
$$K_{ac}^{ij} = \frac{1}{2} [N^i]_{,\xi}^b E_{abcd} [N^j]_{,\xi}^d$$

$$K_{11} = \frac{1}{2} [N^1]_{,\xi}^b E_{1b1d} [N^1]_{,\xi}^d$$

$$= \frac{1}{2} [N^1]_{,\xi}^1 E_{1111} [N^1]_{,\xi}^1$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$

PD PD



$N^1 = \xi$	$N^1_{,\xi} = 1$	$N^1_{,\eta} = 0$
$N^2 = \eta$	$N^2_{,\xi} = 0$	$N^2_{,\eta} = 1$
$N^3 = (1 - \xi - \eta)$	$N^3_{,\xi} = -1$	$N^3_{,\eta}(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

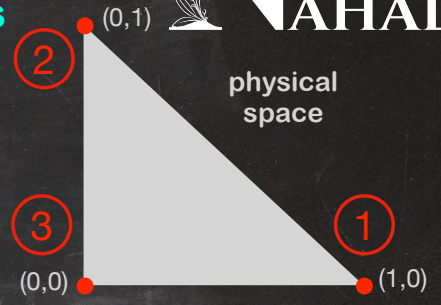


# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$\begin{aligned}
 K_{11}^{11} &= \frac{1}{2} [N_{,\xi}^1]_b E_{1b1d} [N_{,\xi}^1]_d \\
 &= \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1 \\
 &+ \frac{1}{2} [N_{,\xi}^1]_1 E_{1112} [N_{,\xi}^1]_2
 \end{aligned}$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

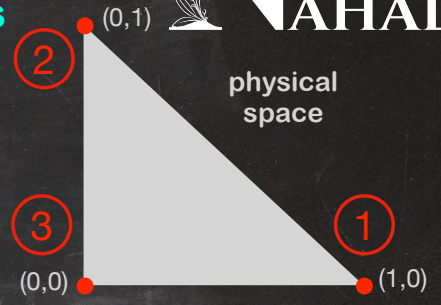


# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$\begin{aligned}
 K_{11} &= \frac{1}{2} [N_{,\xi}^1]_b E_{1b1d} [N_{,\xi}^1]_d \\
 &= \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1 \\
 &\quad + \frac{1}{2} [N_{,\xi}^1]_1 E_{1112} [N_{,\xi}^1]_2 \\
 &\quad + \frac{1}{2} [N_{,\xi}^1]_2 E_{1211} [N_{,\xi}^1]_1
 \end{aligned}$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

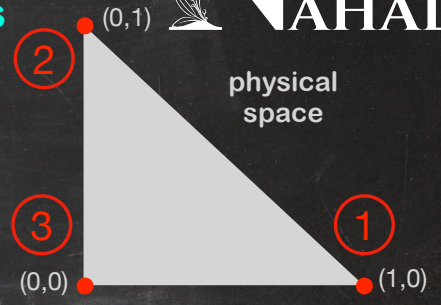
$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$\begin{aligned}
 K_{11}^{11} &= \frac{1}{2} [N_{,\xi}^1]_b E_{1b1d} [N_{,\xi}^1]_d \\
 &= \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1 \\
 &\quad + \frac{1}{2} [N_{,\xi}^1]_1 E_{1112} [N_{,\xi}^1]_2 \\
 &\quad + \frac{1}{2} [N_{,\xi}^1]_2 E_{1211} [N_{,\xi}^1]_1 \\
 &\quad + \frac{1}{2} [N_{,\xi}^1]_2 E_{1212} [N_{,\xi}^1]_2
 \end{aligned}$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$K_{11} = \frac{1}{2} [N_{,\xi}^1]_b E_{1b1d} [N_{,\xi}^1]_d$$

$$= \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1$$

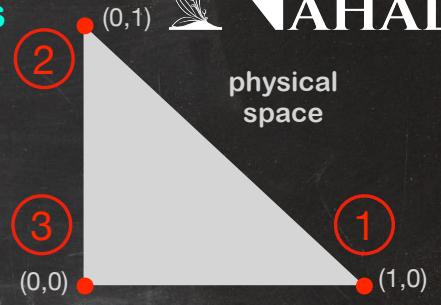
$$+ \frac{1}{2} [N_{,\xi}^1]_1 E_{1112} [N_{,\xi}^1]_2$$

$$+ \frac{1}{2} [N_{,\xi}^1]_2 E_{1211} [N_{,\xi}^1]_1$$

$$+ \frac{1}{2} [N_{,\xi}^1]_2 E_{1212} [N_{,\xi}^1]_2$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$

PD PD



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$



# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$K_{11} = \frac{1}{2} [N_{,\xi}^1]_b E_{1b1d} [N_{,\xi}^1]_d$$

$$= \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1$$

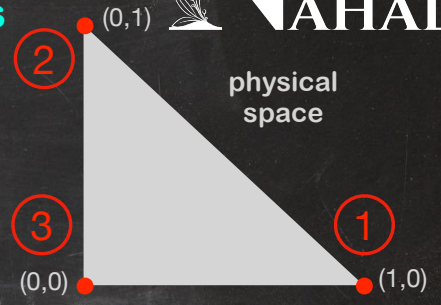
$$+ \frac{1}{2} [N_{,\xi}^1]_1 E_{1112} [N_{,\xi}^1]_2$$

$$+ \frac{1}{2} [N_{,\xi}^1]_2 E_{1211} [N_{,\xi}^1]_1$$

$$+ \frac{1}{2} [N_{,\xi}^1]_2 E_{1212} [N_{,\xi}^1]_2$$

$$\sum_{b=1}^2 \sum_{d=1}^2$$

PD PD



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$

$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$

$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$
$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$

$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$
$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$
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# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$K_{11}^{11} = \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1 + \frac{1}{2} [N_{,\xi}^1]_2 E_{1212} [N_{,\xi}^1]_2$$

$$E_{1111} = E/[1-\nu^2]$$

$$E_{1212} = E/2[1+\nu]$$



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N_{,\xi}^i]_b E_{abcd} [N_{,\xi}^j]_d$$

$$E_{1111} = E/[1-\nu^2]$$

$$E_{1212} = E/2[1+\nu]$$

$$K_{11} = \frac{1}{2} [N_{,\xi}^1]_1 E_{1111} [N_{,\xi}^1]_1$$

$$+ \frac{1}{2} [N_{,\xi}^1]_2 E_{1212} [N_{,\xi}^1]_2$$

$$[N_{,\xi}^1] = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \Rightarrow [N_{,\xi}^1]_1 = 1, [N_{,\xi}^1]_2 = 0$$



$N^1 = \xi$	$N_{,\xi}^1 = 1$	$N_{,\eta}^1 = 0$
$N^2 = \eta$	$N_{,\xi}^2 = 0$	$N_{,\eta}^2 = 1$
$N^3 = (1 - \xi - \eta)$	$N_{,\xi}^3 = -1$	$N_{,\eta}^3(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$

$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$

$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$
$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$

$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$
$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$
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## Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N^i]_{,\xi} E_{abcd} [N^j]_{,\xi} d$$

$$E_{1111} = E/[1-\nu^2]$$

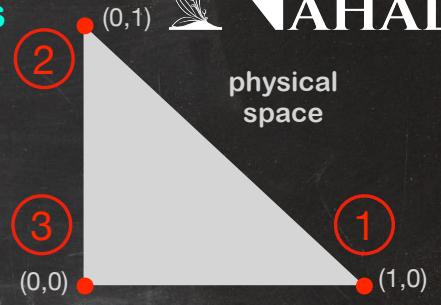
$$E_{1212} = E/2[1+\nu]$$

$$K_{11} = \frac{1}{2} [N^1]_{,\xi} E_{1111} [N^1]_{,\xi} + \frac{1}{2} [N^1]_{,\xi} E_{1212} [N^1]_{,\xi}$$

$$+ \frac{1}{2} [N^1]_{,\xi} E_{1212} [N^1]_{,\xi}$$

$$[N^1]_{,\xi} = 1$$

$$[N^1]_{,\xi} = 0$$



$N^1 = \xi$	$N^1_{,\xi} = 1$	$N^1_{,\eta} = 0$
$N^2 = \eta$	$N^2_{,\xi} = 0$	$N^2_{,\eta} = 1$
$N^3 = (1 - \xi - \eta)$	$N^3_{,\xi} = -1$	$N^3_{,\eta}(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$

$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
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$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
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$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$
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$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
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$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$
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$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$
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# Example (D2TR3N) ... constant strain triangle ... stiffness

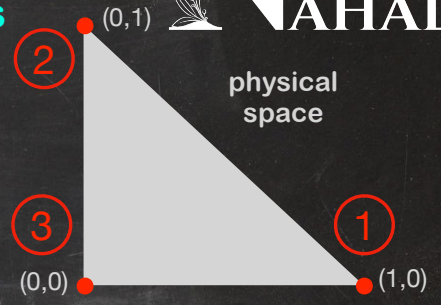
$$K_{ac}^{ij} = \frac{1}{2} [N^i]_b E_{abcd} [N^j]_d$$

$$E_{1111} = E/[1-\nu^2]$$

$$E_{1212} = E/2[1+\nu]$$

$$K_{11} = \frac{1}{2} [N^1]_1 E_{1111} [N^1]_1 + \frac{1}{2} [N^1]_2 E_{1212} [N^1]_2$$

$$= \frac{1}{2} E_{1111} = \frac{E}{2[1-\nu^2]}$$



$N^1 = \xi$	$N^1_{,\xi} = 1$	$N^1_{,\eta} = 0$
$N^2 = \eta$	$N^2_{,\xi} = 0$	$N^2_{,\eta} = 1$
$N^3 = (1 - \xi - \eta)$	$N^3_{,\xi} = -1$	$N^3_{,\eta}(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

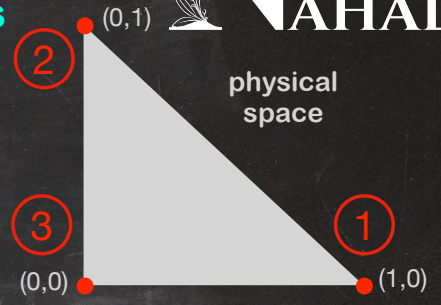


# Example (D2TR3N) ... constant strain triangle ... stiffness

$$K_{ac}^{ij} = \frac{1}{2} [N^i]_{,\xi}{}_b E_{abcd} [N^j]_{,\xi}{}_d$$

$$K_{11}^{11} = \frac{1}{2} E_{4111}$$

$$K_{11}^{11} = \frac{E}{2[1-\nu^2]}$$



$N^1 = \xi$	$N^1_{,\xi} = 1$	$N^1_{,\eta} = 0$
$N^2 = \eta$	$N^2_{,\xi} = 0$	$N^2_{,\eta} = 1$
$N^3 = (1 - \xi - \eta)$	$N^3_{,\xi} = -1$	$N^3_{,\eta}(\xi, \eta) = -1$

$E_{1111} = \frac{E}{1-\nu^2}$	$E_{1112} = 0$	$E_{1121} = 0$	$E_{1122} = \frac{E\nu}{1-\nu^2}$
$E_{1211} = 0$	$E_{1212} = \frac{E}{2[1+\nu]}$	$E_{1221} = \frac{E}{2[1+\nu]}$	$E_{1222} = 0$
$E_{2111} = 0$	$E_{2112} = \frac{E}{2[1+\nu]}$	$E_{2121} = \frac{E}{2[1+\nu]}$	$E_{2122} = 0$
$E_{2211} = \frac{E\nu}{1-\nu^2}$	$E_{2212} = 0$	$E_{2221} = 0$	$E_{2222} = \frac{E}{1-\nu^2}$

# Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix} = \frac{E}{2[1-\nu^2]} \begin{bmatrix} K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\ K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\ K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\ K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\ K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\ K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

**! ATTENTION !**

element stiffness matrix is symmetric and its determinant is zero

## Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix} = \begin{bmatrix} K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\ K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\ K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\ K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\ K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\ K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

**! ATTENTION !**

element stiffness matrix is symmetric and its determinant is zero



## Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} \\ K^{21} & K^{22} & K^{23} \\ K^{31} & K^{32} & K^{33} \end{bmatrix} = \begin{bmatrix} \boxed{K_{11}^{11} \quad K_{12}^{11}} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\ \boxed{K_{21}^{11} \quad K_{22}^{11}} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\ \boxed{K_{11}^{21} \quad K_{12}^{21}} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\ \boxed{K_{21}^{21} \quad K_{22}^{21}} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\ \boxed{K_{11}^{31} \quad K_{12}^{31}} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\ \boxed{K_{21}^{31} \quad K_{22}^{31}} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

**! ATTENTION !**

element stiffness matrix is symmetric and its determinant is zero



## Example (D2TR3N) ... linear triangular element

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K_{11}^{11} = \frac{E}{2[1-\nu^2]}$$

$$K_{12}^{11} = 0$$

$$K_{21}^{11} = 0$$

$$K_{22}^{11} = \frac{E}{4[1+\nu]}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$x^1 = [1, 0]$$

$$x^2 = [0, 1]$$

$$x^3 = [0, 0]$$

## Example (D2TR3N) ... linear triangular element

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K_{11}^{21} = 0$$

$$K_{12}^{21} = \frac{E}{4[1+\nu]}$$

$$K_{21}^{21} = \frac{E\nu}{2[1-\nu^2]}$$

$$K_{22}^{21} = 0$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$x^1 = [1, 0]$$

$$x^2 = [0, 1]$$

$$x^3 = [0, 0]$$

## Example (D2TR3N) ... linear triangular element

Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K_{11}^{31} = - \frac{E}{2[1-\nu^2]}$$

$$K_{12}^{31} = - \frac{E}{4[1+\nu]}$$

$$K_{21}^{31} = - \frac{E\nu}{2[1-\nu^2]}$$

$$K_{22}^{31} = - \frac{E}{4[1+\nu]}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$x^1 = [1, 0]$$

$$x^2 = [0, 1]$$

$$x^3 = [0, 0]$$



## Example (D2TR3N) ... linear triangular element

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$\mathbf{K} = \begin{bmatrix} \frac{E}{2[1-\nu^2]} & 0 & 0 & \frac{E\nu}{2[1-\nu^2]} & -\frac{E}{2[1-\nu^2]} & -\frac{E\nu}{2[1-\nu^2]} \\ 0 & \frac{E}{4[\nu+1]} & \frac{E}{4[\nu+1]} & 0 & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} \\ 0 & \frac{E}{4[\nu+1]} & \frac{E}{4[\nu+1]} & 0 & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} \\ \frac{E\nu}{2[1-\nu^2]} & 0 & 0 & \frac{E}{2[1-\nu^2]} & -\frac{E\nu}{2[1-\nu^2]} & -\frac{E}{2[1-\nu^2]} \\ -\frac{E}{2[1-\nu^2]} & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} & -\frac{E\nu}{2[1-\nu^2]} & \frac{E[3-\nu]}{4[1-\nu^2]} & \frac{E}{4[1-\nu]} \\ -\frac{E\nu}{2[1-\nu^2]} & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} & -\frac{E}{2[1-\nu^2]} & \frac{E}{4[1-\nu]} & \frac{E[3-\nu]}{4[1-\nu^2]} \end{bmatrix}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$



## Example (D2TR3N) ... constant strain triangle ... stiffness

Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{K} = \begin{bmatrix} \mathbf{K}^{11} & \mathbf{K}^{12} & \mathbf{K}^{13} \\ \mathbf{K}^{21} & \mathbf{K}^{22} & \mathbf{K}^{23} \\ \mathbf{K}^{31} & \mathbf{K}^{32} & \mathbf{K}^{33} \end{bmatrix} = \begin{bmatrix} K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} \\ K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} \\ K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} \\ K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} \\ K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} \\ K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

**! ATTENTION !**

element stiffness matrix is symmetric and its determinant is zero

## Example (D2TR3N) ... linear triangular element

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$\mathbf{K} = \begin{bmatrix} \frac{E}{2[1-\nu^2]} & 0 & 0 & \frac{E\nu}{2[1-\nu^2]} & -\frac{E}{2[1-\nu^2]} & -\frac{E\nu}{2[1-\nu^2]} \\ 0 & \frac{E}{4[\nu+1]} & \frac{E}{4[\nu+1]} & 0 & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} \\ 0 & \frac{E}{4[\nu+1]} & \frac{E}{4[\nu+1]} & 0 & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} \\ \frac{E\nu}{2[1-\nu^2]} & 0 & 0 & \frac{E}{2[1-\nu^2]} & -\frac{E\nu}{2[1-\nu^2]} & -\frac{E}{2[1-\nu^2]} \\ -\frac{E}{2[1-\nu^2]} & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} & -\frac{E\nu}{2[1-\nu^2]} & \frac{E[3-\nu]}{4[1-\nu^2]} & \frac{E}{4[1-\nu]} \\ -\frac{E\nu}{2[1-\nu^2]} & -\frac{E}{4[\nu+1]} & -\frac{E}{4[\nu+1]} & -\frac{E}{2[1-\nu^2]} & \frac{E}{4[1-\nu]} & \frac{E[3-\nu]}{4[1-\nu^2]} \end{bmatrix}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{\text{NPE}} \\ y^1 & y^2 & \dots & y^{\text{NPE}} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{\text{NPE}} & N_{\eta}^{\text{NPE}} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$

## Example (D2TR3N) ... linear triangular element

... using one Gauss point ...

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det}\mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$\mathbf{K} = \begin{bmatrix} 5.000 & 0.000 & 0.000 & 0.000 & -5.000 & 0.000 \\ 0.000 & 2.500 & 2.500 & 0.000 & -2.500 & -2.500 \\ 0.000 & 2.500 & 2.500 & 0.000 & -2.500 & -2.500 \\ 0.000 & 0.000 & 0.000 & 5.000 & 0.000 & -5.000 \\ -5.000 & -2.500 & -2.500 & 0.000 & 7.500 & 2.500 \\ 0.000 & -2.500 & -2.500 & -5.000 & 2.500 & 7.500 \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$

$$E = 10, \nu = 0$$



## Example (D2TR3N) ... linear triangular element

... using one Gauss point ...

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det}\mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 5.333 & 0.000 & 0.000 & 1.333 & -5.333 & -1.333 \\ 0.000 & 2.000 & 2.000 & 0.000 & -2.000 & -2.000 \\ 0.000 & 2.000 & 2.000 & 0.000 & -2.000 & -2.000 \\ 1.333 & 0.000 & 0.000 & 5.333 & -1.333 & -5.333 \\ -5.333 & -2.000 & -2.000 & -1.333 & 7.333 & 3.333 \\ -1.333 & -2.000 & -2.000 & -5.333 & 3.333 & 7.333 \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$

$$E = 10, \nu = 0.25$$

## Example (D2TR3N) ... linear triangular element

... using one Gauss point ...

Triangular  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det}\mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad}\delta_{bc} + \delta_{ac}\delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab}\delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 6.667 & 0.000 & 0.000 & 3.333 & -6.667 & -3.333 \\ 0.000 & 1.667 & 1.667 & 0.000 & -1.667 & -1.667 \\ 0.000 & 1.667 & 1.667 & 0.000 & -1.667 & -1.667 \\ 3.333 & 0.000 & 0.000 & 6.667 & -3.333 & -6.667 \\ -6.667 & -1.667 & -1.667 & -3.333 & 8.333 & 5.000 \\ -3.333 & -1.667 & -1.667 & -6.667 & 5.000 & 8.333 \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$

$$E = 10, \nu = 0.5$$

## Example (D2TR3N) ... linear triangular element

... using one Gauss point ...

Triangular Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [\mathbf{J}^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [\mathbf{J}^{-T} \cdot N_{,\xi}^j]_d \text{Det} \mathbf{J} \alpha_{gp} \times \frac{1}{2}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$\mathbf{K} = \begin{bmatrix} 11.429 & 0.000 & 0.000 & 8.571 & -11.429 & -8.571 \\ 0.000 & 1.429 & 1.429 & 0.000 & -1.429 & -1.429 \\ 0.000 & 1.429 & 1.429 & 0.000 & -1.429 & -1.429 \\ 8.571 & 0.000 & 0.000 & 11.429 & -8.571 & -11.429 \\ -11.429 & -1.429 & -1.429 & -8.571 & 12.857 & 10.000 \\ -8.571 & -1.429 & -1.429 & -11.429 & 10.000 & 12.857 \end{bmatrix}$$

$$\mathbf{J} = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [1, 0]$$

$$\mathbf{x}^2 = [0, 1]$$

$$\mathbf{x}^3 = [0, 0]$$

$$E = 10, \nu = 0.75$$



# Example (D2QU4N) ... bilinear quadrilateral element

Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} K^{11} & K^{12} & K^{13} & K^{14} \\ K^{21} & K^{22} & K^{23} & K^{24} \\ K^{31} & K^{32} & K^{33} & K^{34} \\ K^{41} & K^{42} & K^{43} & K^{44} \end{bmatrix} = \begin{bmatrix} K_{11}^{11} & K_{12}^{11} & K_{11}^{12} & K_{12}^{12} & K_{11}^{13} & K_{12}^{13} & K_{11}^{14} & K_{12}^{14} \\ K_{21}^{11} & K_{22}^{11} & K_{21}^{12} & K_{22}^{12} & K_{21}^{13} & K_{22}^{13} & K_{21}^{14} & K_{22}^{14} \\ K_{11}^{21} & K_{12}^{21} & K_{11}^{22} & K_{12}^{22} & K_{11}^{23} & K_{12}^{23} & K_{11}^{24} & K_{12}^{24} \\ K_{21}^{21} & K_{22}^{21} & K_{21}^{22} & K_{22}^{22} & K_{21}^{23} & K_{22}^{23} & K_{21}^{24} & K_{22}^{24} \\ K_{11}^{31} & K_{12}^{31} & K_{11}^{32} & K_{12}^{32} & K_{11}^{33} & K_{12}^{33} & K_{11}^{34} & K_{12}^{34} \\ K_{21}^{31} & K_{22}^{31} & K_{21}^{32} & K_{22}^{32} & K_{21}^{33} & K_{22}^{33} & K_{21}^{34} & K_{22}^{34} \\ K_{11}^{41} & K_{12}^{41} & K_{11}^{42} & K_{12}^{42} & K_{11}^{43} & K_{12}^{43} & K_{11}^{44} & K_{12}^{44} \\ K_{21}^{41} & K_{22}^{41} & K_{21}^{42} & K_{22}^{42} & K_{21}^{43} & K_{22}^{43} & K_{21}^{44} & K_{22}^{44} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

**! ATTENTION !**  
element stiffness matrix is symmetric and its determinant is zero

# Example (D2QU4N) ... bilinear quadrilateral element

... using one Gauss point ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

plane strain

$$+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$K = \begin{bmatrix} \frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} \\ -\frac{E}{8[\nu-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} \\ \frac{E}{8[\nu-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} \\ \frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} \\ \frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} \\ \frac{E}{8[\nu-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} \\ -\frac{E}{8[\nu-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & -\frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} \\ \frac{E[1-3\nu]}{8[\nu^2-1]} & \frac{E}{8[\nu-1]} & -\frac{E}{8[\nu-1]} & -\frac{E[\nu-3]}{8[\nu^2-1]} & \frac{E[1-3\nu]}{8[\nu^2-1]} & -\frac{E}{8[\nu-1]} & \frac{E}{8[\nu-1]} & \frac{E[\nu-3]}{8[\nu^2-1]} \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [-1, -1]$$

$$\mathbf{x}^2 = [1, -1]$$

$$\mathbf{x}^3 = [1, 1]$$

$$\mathbf{x}^4 = [-1, 1]$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using one Gauss point ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 3.750 & 1.250 & -1.250 & -1.250 & -3.750 & -1.250 & 1.250 & 1.250 \\ 1.250 & 3.750 & 1.250 & 1.250 & -1.250 & -3.750 & -1.250 & -1.250 \\ -1.250 & 1.250 & 3.750 & -1.250 & 1.250 & -1.250 & -3.750 & 1.250 \\ -1.250 & 1.250 & -1.250 & 3.750 & 1.250 & -1.250 & 1.250 & -3.750 \\ -3.750 & -1.250 & 1.250 & 1.250 & 3.750 & 1.250 & -1.250 & -1.250 \\ -1.250 & -3.750 & -1.250 & -1.250 & 1.250 & 3.750 & 1.250 & 1.250 \\ 1.250 & -1.250 & -3.750 & 1.250 & -1.250 & 1.250 & 3.750 & -1.250 \\ 1.250 & -1.250 & 1.250 & -3.750 & -1.250 & 1.250 & -1.250 & 3.750 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using four Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 5.000 & 1.250 & -2.500 & -1.250 & -2.500 & -1.250 & 0.000 & 1.250 \\ 1.250 & 5.000 & 1.250 & -0.000 & -1.250 & -2.500 & -1.250 & -2.500 \\ -2.500 & 1.250 & 5.000 & -1.250 & 0.000 & -1.250 & -2.500 & 1.250 \\ -1.250 & -0.000 & -1.250 & 5.000 & 1.250 & -2.500 & 1.250 & -2.500 \\ -2.500 & -1.250 & 0.000 & 1.250 & 5.000 & 1.250 & -2.500 & -1.250 \\ -1.250 & -2.500 & -1.250 & -2.500 & 1.250 & 5.000 & 1.250 & -0.000 \\ 0.000 & -1.250 & -2.500 & 1.250 & -2.500 & 1.250 & 5.000 & -1.250 \\ 1.250 & -2.500 & 1.250 & -2.500 & -1.250 & -0.000 & -1.250 & 5.000 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using nine Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 5.000 & 1.250 & -2.500 & -1.250 & -2.500 & -1.250 & -0.000 & 1.250 \\ 1.250 & 5.000 & 1.250 & -0.000 & -1.250 & -2.500 & -1.250 & -2.500 \\ -2.500 & 1.250 & 5.000 & -1.250 & -0.000 & -1.250 & -2.500 & 1.250 \\ -1.250 & -0.000 & -1.250 & 5.000 & 1.250 & -2.500 & 1.250 & -2.500 \\ -2.500 & -1.250 & -0.000 & 1.250 & 5.000 & 1.250 & -2.500 & -1.250 \\ -1.250 & -2.500 & -1.250 & -2.500 & 1.250 & 5.000 & 1.250 & -0.000 \\ -0.000 & -1.250 & -2.500 & 1.250 & -2.500 & 1.250 & 5.000 & -1.250 \\ 1.250 & -2.500 & 1.250 & -2.500 & -1.250 & -0.000 & -1.250 & 5.000 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using one Gauss point ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 3.667 & 1.667 & -1.667 & -0.333 & -3.667 & -1.667 & 1.667 & 0.333 \\ 1.667 & 3.667 & 0.333 & 1.667 & -1.667 & -3.667 & -0.333 & -1.667 \\ -1.667 & 0.333 & 3.667 & -1.667 & 1.667 & -0.333 & -3.667 & 1.667 \\ -0.333 & 1.667 & -1.667 & 3.667 & 0.333 & -1.667 & 1.667 & -3.667 \\ -3.667 & -1.667 & 1.667 & 0.333 & 3.667 & 1.667 & -1.667 & -0.333 \\ -1.667 & -3.667 & -0.333 & -1.667 & 1.667 & 3.667 & 0.333 & 1.667 \\ 1.667 & -0.333 & -3.667 & 1.667 & -1.667 & 0.333 & 3.667 & -1.667 \\ 0.333 & -1.667 & 1.667 & -3.667 & -0.333 & 1.667 & -1.667 & 3.667 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\begin{aligned} \mathbf{x}^1 &= [-1, -1] \\ \mathbf{x}^2 &= [1, -1] \\ \mathbf{x}^3 &= [1, 1] \\ \mathbf{x}^4 &= [-1, 1] \end{aligned}$$

$$E = 10, \nu = 0.25$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using four Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 4.889 & 1.667 & -2.889 & -0.333 & -2.444 & -1.667 & 0.444 & 0.333 \\ 1.667 & 4.889 & 0.333 & 0.444 & -1.667 & -2.444 & -0.333 & -2.889 \\ -2.889 & 0.333 & 4.889 & -1.667 & 0.444 & -0.333 & -2.444 & 1.667 \\ -0.333 & 0.444 & -1.667 & 4.889 & 0.333 & -2.889 & 1.667 & -2.444 \\ -2.444 & -1.667 & 0.444 & 0.333 & 4.889 & 1.667 & -2.889 & -0.333 \\ -1.667 & -2.444 & -0.333 & -2.889 & 1.667 & 4.889 & 0.333 & 0.444 \\ 0.444 & -0.333 & -2.444 & 1.667 & -2.889 & 0.333 & 4.889 & -1.667 \\ 0.333 & -2.889 & 1.667 & -2.444 & -0.333 & 0.444 & -1.667 & 4.889 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\begin{aligned} \mathbf{x}^1 &= [-1, -1] \\ \mathbf{x}^2 &= [1, -1] \\ \mathbf{x}^3 &= [1, 1] \\ \mathbf{x}^4 &= [-1, 1] \end{aligned}$$

$$E = 10, \nu = 0.25$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using nine Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 4.889 & 1.667 & -2.889 & -0.333 & -2.444 & -1.667 & 0.444 & 0.333 \\ 1.667 & 4.889 & 0.333 & 0.444 & -1.667 & -2.444 & -0.333 & -2.889 \\ -2.889 & 0.333 & 4.889 & -1.667 & 0.444 & -0.333 & -2.444 & 1.667 \\ -0.333 & 0.444 & -1.667 & 4.889 & 0.333 & -2.889 & 1.667 & -2.444 \\ -2.444 & -1.667 & 0.444 & 0.333 & 4.889 & 1.667 & -2.889 & -0.333 \\ -1.667 & -2.444 & -0.333 & -2.889 & 1.667 & 4.889 & 0.333 & 0.444 \\ 0.444 & -0.333 & -2.444 & 1.667 & -2.889 & 0.333 & 4.889 & -1.667 \\ 0.333 & -2.889 & 1.667 & -2.444 & -0.333 & 0.444 & -1.667 & 4.889 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\begin{aligned} \mathbf{x}^1 &= [-1, -1] \\ \mathbf{x}^2 &= [1, -1] \\ \mathbf{x}^3 &= [1, 1] \\ \mathbf{x}^4 &= [-1, 1] \end{aligned}$$

$$E = 10, \nu = 0.25$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using one Gauss point ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 4.167 & 2.500 & -2.500 & 0.833 & -4.167 & -2.500 & 2.500 & -0.833 \\ 2.500 & 4.167 & -0.833 & 2.500 & -2.500 & -4.167 & 0.833 & -2.500 \\ -2.500 & -0.833 & 4.167 & -2.500 & 2.500 & 0.833 & -4.167 & 2.500 \\ 0.833 & 2.500 & -2.500 & 4.167 & -0.833 & -2.500 & 2.500 & -4.167 \\ -4.167 & -2.500 & 2.500 & -0.833 & 4.167 & 2.500 & -2.500 & 0.833 \\ -2.500 & -4.167 & 0.833 & -2.500 & 2.500 & 4.167 & -0.833 & 2.500 \\ 2.500 & 0.833 & -4.167 & 2.500 & -2.500 & -0.833 & 4.167 & -2.500 \\ -0.833 & -2.500 & 2.500 & -4.167 & 0.833 & 2.500 & -2.500 & 4.167 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0.5$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using four Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 5.556 & 2.500 & -3.889 & 0.833 & -2.778 & -2.500 & 1.111 & -0.833 \\ 2.500 & 5.556 & -0.833 & 1.111 & -2.500 & -2.778 & 0.833 & -3.889 \\ -3.889 & -0.833 & 5.556 & -2.500 & 1.111 & 0.833 & -2.778 & 2.500 \\ 0.833 & 1.111 & -2.500 & 5.556 & -0.833 & -3.889 & 2.500 & -2.778 \\ -2.778 & -2.500 & 1.111 & -0.833 & 5.556 & 2.500 & -3.889 & 0.833 \\ -2.500 & -2.778 & 0.833 & -3.889 & 2.500 & 5.556 & -0.833 & 1.111 \\ 1.111 & 0.833 & -2.778 & 2.500 & -3.889 & -0.833 & 5.556 & -2.500 \\ -0.833 & -3.889 & 2.500 & -2.778 & 0.833 & 1.111 & -2.500 & 5.556 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0.5$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using nine Gauss points ...

Quadrilateral  
Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}] + \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

plane strain

$$K = \begin{bmatrix} 5.556 & 2.500 & -3.889 & 0.833 & -2.778 & -2.500 & 1.111 & -0.833 \\ 2.500 & 5.556 & -0.833 & 1.111 & -2.500 & -2.778 & 0.833 & -3.889 \\ -3.889 & -0.833 & 5.556 & -2.500 & 1.111 & 0.833 & -2.778 & 2.500 \\ 0.833 & 1.111 & -2.500 & 5.556 & -0.833 & -3.889 & 2.500 & -2.778 \\ -2.778 & -2.500 & 1.111 & -0.833 & 5.556 & 2.500 & -3.889 & 0.833 \\ -2.500 & -2.778 & 0.833 & -3.889 & 2.500 & 5.556 & -0.833 & 1.111 \\ 1.111 & 0.833 & -2.778 & 2.500 & -3.889 & -0.833 & 5.556 & -2.500 \\ -0.833 & -3.889 & 2.500 & -2.778 & 0.833 & 1.111 & -2.500 & 5.556 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

- $\mathbf{x}^1 = [-1, -1]$
- $\mathbf{x}^2 = [1, -1]$
- $\mathbf{x}^3 = [1, 1]$
- $\mathbf{x}^4 = [-1, 1]$

$$E = 10, \nu = 0.5$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using one Gauss point ...

Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det}J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

plane strain

$$+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$K = \begin{bmatrix} 6.429 & 5.000 & -5.000 & 3.571 & -6.429 & -5.000 & 5.000 & -3.571 \\ 5.000 & 6.429 & -3.571 & 5.000 & -5.000 & -6.429 & 3.571 & -5.000 \\ -5.000 & -3.571 & 6.429 & -5.000 & 5.000 & 3.571 & -6.429 & 5.000 \\ 3.571 & 5.000 & -5.000 & 6.429 & -3.571 & -5.000 & 5.000 & -6.429 \\ -6.429 & -5.000 & 5.000 & -3.571 & 6.429 & 5.000 & -5.000 & 3.571 \\ -5.000 & -6.429 & 3.571 & -5.000 & 5.000 & 6.429 & -3.571 & 5.000 \\ 5.000 & 3.571 & -6.429 & 5.000 & -5.000 & -3.571 & 6.429 & -5.000 \\ -3.571 & -5.000 & 5.000 & -6.429 & 3.571 & 5.000 & -5.000 & 6.429 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [-1, -1]$$

$$\mathbf{x}^2 = [1, -1]$$

$$\mathbf{x}^3 = [1, 1]$$

$$\mathbf{x}^4 = [-1, 1]$$

$$E = 10, \nu = 0.75$$



# Example (D2QU4N) ... bilinear quadrilateral element

... using four Gauss points ...

Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

plane strain

$$+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$K = \begin{bmatrix} 8.571 & 5.000 & -7.143 & 3.571 & -4.286 & -5.000 & 2.857 & -3.571 \\ 5.000 & 8.571 & -3.571 & 2.857 & -5.000 & -4.286 & 3.571 & -7.143 \\ -7.143 & -3.571 & 8.571 & -5.000 & 2.857 & 3.571 & -4.286 & 5.000 \\ 3.571 & 2.857 & -5.000 & 8.571 & -3.571 & -7.143 & 5.000 & -4.286 \\ -4.286 & -5.000 & 2.857 & -3.571 & 8.571 & 5.000 & -7.143 & 3.571 \\ -5.000 & -4.286 & 3.571 & -7.143 & 5.000 & 8.571 & -3.571 & 2.857 \\ 2.857 & 3.571 & -4.286 & 5.000 & -7.143 & -3.571 & 8.571 & -5.000 \\ -3.571 & -7.143 & 5.000 & -4.286 & 3.571 & 2.857 & -5.000 & 8.571 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [-1, -1]$$

$$\mathbf{x}^2 = [1, -1]$$

$$\mathbf{x}^3 = [1, 1]$$

$$\mathbf{x}^4 = [-1, 1]$$

$$E = 10, \nu = 0.75$$

# Example (D2QU4N) ... bilinear quadrilateral element

... using nine Gauss points ...

Quadrilateral Elements

$$K_{ac}^{ij} = \sum_{gp=1}^{GPE} [J^{-T} \cdot N_{,\xi}^i]_b E_{abcd} [J^{-T} \cdot N_{,\xi}^j]_d \text{Det} J \alpha_{gp}$$

$$E_{abcd} = \frac{E}{2[1+\nu]} [\delta_{ad} \delta_{bc} + \delta_{ac} \delta_{bd}]$$

plane strain

$$+ \frac{E\nu}{1-\nu^2} \delta_{ab} \delta_{cd}$$

$$K = \begin{bmatrix} 8.571 & 5.000 & -7.143 & 3.571 & -4.286 & -5.000 & 2.857 & -3.571 \\ 5.000 & 8.571 & -3.571 & 2.857 & -5.000 & -4.286 & 3.571 & -7.143 \\ -7.143 & -3.571 & 8.571 & -5.000 & 2.857 & 3.571 & -4.286 & 5.000 \\ 3.571 & 2.857 & -5.000 & 8.571 & -3.571 & -7.143 & 5.000 & -4.286 \\ -4.286 & -5.000 & 2.857 & -3.571 & 8.571 & 5.000 & -7.143 & 3.571 \\ -5.000 & -4.286 & 3.571 & -7.143 & 5.000 & 8.571 & -3.571 & 2.857 \\ 2.857 & 3.571 & -4.286 & 5.000 & -7.143 & -3.571 & 8.571 & -5.000 \\ -3.571 & -7.143 & 5.000 & -4.286 & 3.571 & 2.857 & -5.000 & 8.571 \end{bmatrix}$$

$$J = \begin{bmatrix} x^1 & x^2 & \dots & x^{NPE} \\ y^1 & y^2 & \dots & y^{NPE} \end{bmatrix} \begin{bmatrix} N_{\xi}^1 & N_{\eta}^1 \\ N_{\xi}^2 & N_{\eta}^2 \\ \vdots & \vdots \\ N_{\xi}^{NPE} & N_{\eta}^{NPE} \end{bmatrix}$$

$$\mathbf{x}^1 = [-1, -1]$$

$$\mathbf{x}^2 = [1, -1]$$

$$\mathbf{x}^3 = [1, 1]$$

$$\mathbf{x}^4 = [-1, 1]$$

$$E = 10, \nu = 0.75$$